



Report:

Mercury Emission Testing at the Clean Harbors Sarnia Facility (July 2016)

Date: September 1, 2016





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| Submitted to: | Erica Carabott Facility Compliance Manager Clean Harbors Canada Inc. 4090 Telfer Road, Corunna, Ontario NON 1G0 Tel: (519) 864-3890 Cell: (519) 328-3394 E-mail: <u>carabott.erica@cleanharbors.com</u> |
|---------------|---|
| Prepared by: | Tina Sanderson, B.Sc. Senior Specialist, Emission Testing ORTECH Consulting Inc. 804 Southdown Rd., Mississauga, Ontario L5J 2Y4 Tel: (905) 822-4120, Ext. 522 Email: <u>tsanderson@ortech.ca</u> |
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EXECUTIVE SUMMARY

ORTECH Consulting Inc. (ORTECH) was requested by Clean Harbors Canada Inc., (Clean Harbors) to conduct a mercury emission testing program at the incineration facility located in Corunna, Ontario.

Mercury emission tests were performed at the Incinerator Exhaust Stack following the procedures outlined in US EPA Method 30B, "Determination of Total Vapour Phase Mercury Emissions from Coal-Fired Combustion Sources Using Carbon Sorbent Traps" to determine the amount of total vapour phase mercury present in the gas stream.

The test method states that the recovery spike must be within 50 to 150 percent of the expected mass collected in the traps during sampling. Six pairs of tube samples were collected during one day of testing on July 20, 2016. To ensure that at least one of the spike concentrations would fall within the concentration range requirements of the test method one tube from each of the six pairs of adsorbent tubes were spiked with increasing amounts of mercury, ranging from 100 ng to 2600 ng, by the analytical laboratory prior to commencing the test program.

The results of three of the pairs of tubes, including the spike that best represented the mercury concentration in the stack gas at the time of testing, are reported.

The average combustion gas values for each test period were obtained from the plant continuous emission monitoring (CEM) system. The average oxygen concentration for each test was used to determine the dry reference concentration adjusted to 11% oxygen.

The average mercury emission data from the triplicate total vapour phase mercury tests is provided below:

| Mercury Parameter | Average |
|--|---------|
| Dry Reference Concentration (µg/Rm ³)* | 1.49 |
| Dry Adjusted Concentration (µg/Rm ³)** | 1.24 |

* reference conditions are 25°C and 1 atmosphere

** at 25°C and 1 atmosphere, adjusted to 11% oxygen

During the emission testing program, the powdered activated carbon (PAC) injection rate was 22.6 lb/hr.



1. INTRODUCTION

ORTECH Consulting Inc. (ORTECH) was requested by Clean Harbors Canada Inc., (Clean Harbors) to conduct a mercury emission testing program at the incineration facility located in Corunna, Ontario.

Mercury emission tests were performed at the Incinerator Exhaust Stack following the procedures outlined in US EPA Method 30B, "Determination of Total Vapour Phase Mercury Emissions from Coal-Fired Combustion Sources Using Carbon Sorbent Traps" to determine the amount of total vapour phase mercury present in the gas stream.

The average combustion gas values for each test period were obtained from the plant continuous emission monitoring (CEM) system. The average oxygen concentration for each test was used to determine the dry reference concentration adjusted to 11% oxygen.

Six pairs of adsorbent tubes were collected during one day of sampling on July 20, 2016. The spike tubes from each test pair were spiked with increasing amounts of mercury, ranging from 100 ng to 2600 ng, prior to commencing the test program to ensure that at least one of the spike concentrations would fall within the concentration range requirements of the test method. The test method states that the recovery spike must be within 50 to 150 percent of the expected mass collected in the traps during sampling. The results of three of the pairs of tubes, including the spike that best represented the mercury concentration in the stack gas at the time of testing, are reported.

All tables referenced herein are included in Appendix 1.

2. SAMPLING LOCATION

The Incinerator Exhaust Stack has an inside diameter of 1.52 meters at the sampling platform and 1.22 meters at the stack exit. The stack height above grade is 68.6 meters.

Mercury sampling was conducted at the breeching connecting the induced draft fan to the stack. Sampling was conducted at a single point in the center of the duct.

Previous testing programs conducted by ORTECH at the Clean Harbors Incinerator Exhaust Stack have shown that there is no stack gas stratification between the breeching connecting the induced draft fan to the stack and the stack sampling platform location.



3. SAMPLING METHODOLOGY

Mercury emission tests were performed following the procedures outlined in US EPA Method 30B, "Determination of Total Vapour Phase Mercury Emissions from Coal-Fired Combustion Sources Using Carbon Sorbent Traps".

ORTECH used two probes in parallel so that the mercury traps were only 1 to 2 inches apart. Each probe was heated to approximately 135°C to prevent condensation of the stack gas on the sampling media. Each mercury trap was also specially designed for sampling at wet sources. Each tube had an extended section of glass to allow for the heating of the stack gas before it came into contact with the sampling media.

The sampling methodology is briefly described as follows. Each sorbent trap was removed from the clean sorbent trap storage container, the end caps were removed from the traps and the traps were attached to the end of the sampling probe and leak checked. The probe was inserted into the stack and the sample pumps were started. Stack gas was drawn through the traps and into the sampling probe and the sampled gas stream then passed through a series of empty impingers followed by a silica gel trap to remove any remaining traces of moisture prior to the pump and dry gas meter.

A run consisted of paired mercury traps, identified as either A or B, sampled simultaneously. In each tube pair one of either the A or B tube was spiked with a known quantity of mercury. Due to the variability in the mercury concentration in the stack gas and the necessity to have the spiked tubes prepared at least two weeks in advance of the testing program, six pairs of tubes were used for the sampling program to ensure that at least one of the spike concentrations would fall within the concentration range requirements of the test method.

Each test run was sixty minutes in duration at an approximate sampling rate of one liter per minute.

At approximately five minute time increments throughout each test, the following information was measured and recorded for each sampling train:

- Elapsed sampling time
- Dry gas meter volume
- Dry gas meter temperatures
- Control module orifice pressure
- Sampling pump vacuum



At the start and finish of each sampling run the sampling trains were leak-checked. The leakage rate for each train must not exceed 4% of the average sampling rate for the collection period. If a trap pair did not have an acceptable initial leak check, the leak was found and repaired and/or the traps were replaced with a new pair until no leak was discernible. All the leak checks performed for the traps used showed no discernible leak through the test train.

Field testing data sheets for the mercury tests are provided in Appendix 2.

All of the sampling equipment used during the emission testing program was calibrated following the applicable reference method. Equipment calibration data is provided in Appendix 3.

4. ANALYSIS METHODOLOGY

At the end of each successful sampling run, the mercury traps were removed from the test train, capped and placed in their appropriate sample container. Each trap was labeled prior to being shipped to Ohio Lumex for analysis.

The traps were analyzed by thermal decomposition with atomic absorption following the procedures detailed in US EPA Method 7473 (direct thermal desorption with atomic absorption and no gold amalgamation). The method is applicable for total mercury "direct" testing of 40 CFR Part 75 Appendix K and EPA Method 30B sorbent traps.

The analysis is briefly described as follows. The sorbent trap tube end cap is removed; the glass wool plug closest to the appropriate carbon bed is carefully removed and separated from the carbon fraction. The sorbent is transferred into a quartz ladle and then covered with anhydrous sodium carbonate. The ladle is inserted into the heated analyzer thermo catalytic conversion chamber. Mercury is converted from a bound state to the atomic state by thermal decomposition in the furnace and is then detected by atomic absorption. The mercury concentration is measured and recorded using an automated data acquisition system. Both the glass wool plug and the sorbent of each bed are analyzed for the trap and the final mercury mass is the sum of the measurements.

The Ohio Lumex analytical report for total vapour phase mercury is provided in Appendix 4.



5. QUALITY ASSURANCE/QUALITY CONTROL PROGRAM

The analysis of samples for mercury was performed by thermal decomposition with atomic absorption. Specific analytical QC procedures for the mercury analysis are summarized below:

- Calibrations are performed on the day of the analysis.
- Three or more calibration points are used for the calibration curve.
- The field samples analyzed must fall within a calibrated range.
- For each calibration curve, $R^2 \ge 0.99$, and the analyzer response must be within ± 10% for each standard used in the calibration.
- Following calibration, a second source standard is analyzed. The measured value of the independently prepared standard must be within ± 10% of the expected value.
- A blank analysis is conducted prior to analyzing the samples and must be less than the method detection limit.
- At the end of each set of analysis, a calibration standard is tested which must be within ±10% of the expected value.

Approximately two weeks before the field testing, sample media was ordered from Ohio Lumex. Six unspiked mercury traps and six pre-spiked mercury traps were ordered. The pre-spiked mercury traps were spiked with known quantities of mercury ranging from 100 ng to 2600 ng in order to ensure that at least one of the traps fell within the spiking criterion stated in the test method. The recovery spike must be within 50 to 150 percent of the expected mass collected in the traps during sampling according to the test method. The spiking levels for the field recovery traps was estimated using mercury emission data from previous testing programs conducted between 2014 and 2016. The prespiked mercury trap for Test No. 1 (100 ng) was used for spike recovery determination as the concentrations best fit the requirements of the QA/QC criteria (within \pm 50% of the average mercury collected for Test No. 1, Test No. 2 and Test No. 4 (85.2 ng).

The field spike recovery provides specific verification of the performance of the combined sampling and analytical approach for the test program. Six sets of paired samples, one of each pair which is spiked with a known quantity of mercury, were collected. The samples were analyzed and the spike concentration for Test No. 1 fell within the spike range criterion stated in the test method. The spike recovery for Test No. 1 was 97.4%. US EPA Method 30B requires the spike recovery to be between 85 % and 115%.



US EPA Method 30B requires the paired sorbent trap agreement to be $\leq 10\%$ relative deviation for mercury concentrations greater than 1 µg/Rm³ or $\leq 20\%$ relative deviation for mercury concentrations less than 1 µg/Rm³. If the paired trap agreement is greater than the above stated limits the run is not valid. All of the traps collected during the test program had concentrations greater than 1 µg/Rm³. The average dry adjusted mercury concentration ranged from a low of 1.09 µg/Rm³ to a high of 1.42 µg/Rm³ for the six tests performed. The paired trap agreement was 1.4% for Test No. 1, 9.0% for Test No. 2, and 2.2% for Test No. 4.

6. **RESULTS**

Six mercury runs were collected during one day of sampling on July 20, 2016. A run consisted of paired mercury traps, identified as either A or B, sampled simultaneously. The spike tubes from each test pair were spiked with increasing amounts of mercury, ranging from 100 ng to 2600 ng, prior to commencing the test program to ensure that at least one of the spike concentrations would fall within the concentration range requirements of the test method. The results for Test No. 1, Test No. 2 and Test No. 4 are reported.

The sampling schedule is summarized in Table 1. This information includes test dates and times for each of the mercury runs performed. All test times match plant time (i.e. daylight savings time).

Mercury emission sample analyses for Test No. 1, Test No. 2 and Test No. 4 are provided in Table 3. Mercury was detected in Section 1 of each trap in quantities greater than the method detection limit (0.493 ng) in all of the traps. Mercury was also collected in Section 2 in five of the twelve traps in quantities greater than the method detection limit. However, the amount detected in Section 2 was less than 1.2% of the mercury collected in Section 1, indicating that there was no breakthrough or potential loss of mercury. US EPA Method 30B states that $\leq 10\%$ of the total mercury collected should be collected in Section 2 for mercury concentrations greater than 1 µg/Rm³ or $\leq 20\%$ of the total mercury collected in Section 2 for mercury concentrations less than 1 µg/Rm³.

Included in Table 2 are the mercury concentration calculations for Test No. 1, Test No. 2 and Test No. 4. The average oxygen concentration measured by the Clean Harbors CEM system for each test was used to determine the dry reference concentration adjusted to 11% oxygen.

Approximately two weeks before the field testing, sample media was ordered from Ohio Lumex. Six unspiked mercury traps and six pre-spiked mercury traps were ordered. The pre-spiked mercury traps were spiked with known quantities of mercury ranging from 100 ng to 2600 ng in order to ensure that at least one of the traps fell within the spiking criterion stated in the test method. The pre-spiked mercury trap for Test No. 1 (100 ng) was used for spike recovery determination as the concentration best fit the requirements of the QA/QC criteria (within ±50% of the expected concentration).



US EPA Method 30B states that it is acceptable to use the field recovery runs as test runs for emission testing as long as they meet the paired trap agreement criteria. The mass of the mercury spike initially present in each of the spiked traps was subtracted from the total mercury collected in Section 1 of the trap. The difference represents the amount of mercury in the stack gas.

The paired trap agreement was 1.4% for Test No. 1, 9.0% for Test No. 2, and 2.2% for Test No. 4. The mercury emission data from the total vapour phase mercury tests is provided below:

| Mercury Parameter | Test 1 | Test 2 | Test 4 | Average |
|--|--------|--------|--------|---------|
| Dry Reference Conc. (µg/Rm ³)* | 1.56 | 1.53 | 1.39 | 1.49 |
| Dry Adjusted Conc. (μg/Rm ³)** | 1.30 | 1.25 | 1.18 | 1.24 |

- * Reference conditions are 25°C and 1 atmosphere
- ** At 25°C and 1 atmosphere, adjusted to 11% oxygen

The incinerator exhaust stack mercury concentration limit as stated in Environmental Compliance Approval No. 8-1030-94-006 (formerly Certificate of Approval (Air) No. 8-1030-94-006) is 50 μ g/Rm³ adjusted to 11% oxygen. The mercury concentrations were below this limit during the test program.

The spiked mercury trap recovery calculation for Test No. 1 is shown in Table 3; the spike recovery for Test No. 1 was 97.4. US EPA Method 30B requires the average of the spike recoveries to be between 85% and 115%.

7. FACILITY PROCESS DATA

Incinerator process data was supplied by Clean Harbors personnel for the emission test periods. The process data is provided in Appendix 5 as average values for each test for the following process parameters:

- incinerator feed rates (rich, lean, emulsion and alkaline streams)
- volumetric flowrates (secondary air and stack gases)
- temperatures (primary zone, secondary zone, spray dryer inlet and outlet, stack gases)
- pressures (burner, spray dryer outlet, baghouse differential)
- combustion gas stack concentrations (CO, HCl, CO₂, H₂O, THC, O₂, SO₂)
- stack gas opacity
- carbon injection rate

During the emission testing program, the average powdered activated carbon (PAC) injection rate was 22.6 lb/hr.



APPENDIX 1

Data Tables (2 pages)



Table 1: Mercury Test Schedule

| Test Number | Test Date | Samplin | g Period | Sampling Time |
|----------------|---------------|---------|----------|---------------|
| | | Start | Finish | min |
| 1 | July 20, 2016 | 9:51 | 10:51 | 60 |
| 2 | July 20, 2016 | 11:06 | 12:06 | 60 |
| 3 | July 20, 2016 | 12:21 | 13:21 | 60 |
| 4 | July 20, 2016 | 13:38 | 14:38 | 60 |
| 5 | July 20, 2016 | 14:54 | 15:54 | 60 |
| 6 | July 20, 2016 | 16:05 | 17:05 | 60 |
| | | | | |

Note: All test times match plant time (i.e. daylight savings time).



Table 2: Mercury Emission Data

| Test/Run | Tube | Ν | Aercury Collected | I | Dry Gas | Mercury Co | ncentration | Paired |
|----------|---------|-----------|-------------------|-------|-------------------|----------------------|-----------------------|-------------------|
| No. | ID | Section 1 | Section 2 | Total | Volume Sampled | Dry Reference | Dry Adjusted | Trap Agreement |
| | | ng | ng | ng | Rm ³ * | µg/Rm ³ * | μg/Rm ³ ** | % |
| | | | | | | | | |
| 1 | A *** | 84.2 | 0.2 | 84.4 | 0.0549 | 1.54 | 1.28 | - |
| | В | 93.9 | <0.49 | 93.9 | 0.0594 | 1.58 | 1.31 | - |
| | Average | | | | | 1.56 | 1.30 | 1.4 |
| 2 | A | 91.4 | 1.0 | 92.4 | 0.0555 | 1.66 | 1.36 | - |
| | B *** | 82.4 | 1.3 | 83.7 | 0.0603 | 1.39 | 1.13 | - |
| | Average | | | | | 1.53 | 1.25 | 9.0 |
| 4 | A | 76.3 | <0.49 | 76.3 | 0.0560 | 1.36 | 1.15 | - |
| | B *** | 80.5 | <0.49 | 80.5 | 0.0565 | 1.42 | 1.20 | - |
| | Average | | | | | 1.39 | 1.18 | 2.2 |
| Average | | | | 85.2 | | 1.49 | 1.24 | |

Note: Concentration data is only report for three tests as required by US EPA Method 30B

* At 25°C and 1 atmosphere

** At 25°C and 1 atmosphere, adjusted to 11% oxygen

*** Spiked tube, mercury collected corrected for the original spike (100 ng for Test No. 1, 250 ng for Test No. 2, 800 ng for Test No. 4).

Table 3: Mercury Spike Tube Recovery

| Test | | Spike Tube | | | Unspike Tube | e | Spike | Spike |
|---------|--------------------|-------------------|--------------------------|--------------------|-------------------|--------------------------|----------------------|----------|
| No. | Total Collected | Volume Sampled | Mercury Concentration | Total Collected | Volume Sampled | Mercury Concentration | Concentration | Recovery |
| | ng | Rm ³ * | ng/Rm ³ * | ng | Rm ³ * | ng/Rm ³ * | ng/Rm ³ * | % |
| 1 | 184 | 0.0549 | 3354 | 93.9 | 0.0594 | 1580 | 1774 | 97.4 |
| 2 | 334 | 0.0603 | 5538 | 92.4 | 0.0555 | 1665 | 3874 | NA |
| 4 | 881 | 0.0565 | 15579 | 76.3 | 0.0560 | 1362 | 14216 | NA |
| Average | | | | | | | | 97.4 |

Note: The spike tubes were spiked with mercury by the analytical laboratory prior to sampling. The original spike concentrations were 100 ng for Test No. 1, 250 ng for Test No. 2 and 800 ng for Test No. 4.

"NA" Not Applicable. Spike recovery was not calculated as spike concentration was outside the range specified in US EPA Method 30B.



APPENDIX 2

Mercury Field Data Sheets (7 pages) Clean Harbors, Sarnia Mercury Tube Sampling Train Sample Volume Corrections

Incinerator Exhaust Stack

| Test # - Tube | DGMCF | Initial DGM | Final DGM | Actual Vol. | Barometric | Average DGM | Average DGM | Corrected | Corrected |
|----------------------|-------|-------------|-----------|-------------|------------|-----------------------------|-------------|-----------|-----------|
| (tube pair field ID) | | Reading | Reading | Sampled | Pressure | Pressure | Temperature | Volume | Volume |
| | | (L) | (r) | (L) | (in Hg) | del H (in H ₂ O) | (°C) | (n)* | (Rm³)* |
| T1A OL369249 Spiked | 0.991 | 61.80 | 118.18 | 56.38 | 29.6 | 1.8 | 28.5 | 54.91 | 0.0549 |
| T1B OLC025413 | 0.996 | 84.40 | 145.15 | 60.75 | 29.6 | 1.4 | 28.4 | 59.43 | 0.0594 |
| T2A OLC025459 | 0.991 | 19.92 | 77.60 | 57.68 | 29.6 | 2.0 | 32.2 | 55.51 | 0.0555 |
| T2B OLC013396 Spiked | 0.996 | 47.32 | 109.75 | 62.43 | 29.6 | 1.4 | 32.4 | 60.25 | 0.0603 |
| T3A OL291911 Spiked | 0.991 | 80.98 | 139.51 | 58.53 | 29.6 | 2.0 | 33.5 | 56.07 | 0.0561 |
| T3B OLC025428 | 0.996 | 13.68 | 74.78 | 61.10 | 29.6 | 1.4 | 34.7 | 58.51 | 0.0585 |
| T4A OLC025473 | 0.991 | 46.32 | 104.80 | 58.48 | 29.6 | 2.0 | 33.4 | 56.00 | 0.0560 |
| T4B OL336499 Spiked | 0.996 | 83.17 | 142.00 | 58.83 | 29.6 | 1.4 | 33.5 | 56.52 | 0.0565 |
| T5A OL335287 Spiked | 0.991 | 5.81 | 64.46 | 58.65 | 29.6 | 2.0 | 36.1 | 55.66 | 0.0557 |
| T5B OLC025470 | 0.996 | 43.12 | 106.69 | 63.57 | 29.6 | 1.4 | 35.8 | 60.60 | 0.0606 |
| T6A OLC025479 | 0.991 | 65.86 | 125.81 | 59,95 | 29.6 | 2.0 | 36.3 | 56.81 | 0.0568 |
| T6B OL331414 Spiked | 0.996 | 8.50 | 71.73 | 63.23 | 29.6 | 1.4 | 37.0 | 60.00 | 0.0600 |
| | | | | | | | | | |

* dry at 25°C and 1 atmosphere

| Plant: | Clean Habors | | |
|----------------------------|------------------|-----------------|--|
| Plant Location: | Corunna, Ontario | | |
| Test No.: | 1 | | |
| | | | |
| Train A | | <i>~</i> | |
| Tube Identification: | 01369249 | Spiked (Yes) No | |
| Spike Concentration | 100 1 | ng | |
| | | | |

| Test location: | Stack Breeching |
|------------------|-----------------|
| Date: Tury | 20 2016 |
| Project No.: 🦿 🦿 | 21701 |
| | |

| Measuring Device | MII | | |
|------------------|-----------|--|--|
| Control Module 2 | 10117 | | |
| Barometer | ENV. CAN! | | |

and and a second

Barometric Pressure

1,62

| Clock | Dry Gas | Meter Tem | perature | Meter | Pump |
|----------------------------|---------|-----------|----------|-----------------|--------------------|
| Time | Meter | AUG | Inlet | Pressure Δ H | Vacuum _"Hg |
| an an an Araba An Araba | L | <u>°C</u> | °C | "H₂U | Gauge |
| 0 | 61.90 | 24 | 1 | 1.9 | 2 |
| 5 | 66.0 | 26 | | 1.4 | 3 |
| 10 | 50.6 | 29 | | 1.5 | $\overline{\zeta}$ |
| 15 | 1951 | 21 | - | 1.8 | Ý |
| 20 | 1999 | 28 | | 1.8 | 4.5 |
| 25 | \$4.1 | 29 | | 1.5 | (5 |
| 30 | á4.1 | Z | | 1.8 | 5 |
| 35 | 84.0 | 24 | | 1.9 | 5 |
| 40 | 49.0 | 30 | | 1.4 | 5 |
| 45 | 194.0 | 30 | | 1.5 | 5 |
| 50 | 109.0 | 30 | | 1.5 | 5 |
| 55 | 114.0 | 31 | | 1.8 | 5 |
| 60 | 118.18 | 31 | | 1.5 | |
| | | | | | |

| Start Time: 951 | Initial Leak Check 💪 🕜 | Lpm@ 17'Hg | DGMCF: | 0.991 |
|-------------------|------------------------|---------------------------------------|-------------------|-------|
| Finish Time: 1051 | Final Leak Check 6.0 | (Lpm@ 15"Hg | Sample Volume: | 56.38 |
| | | · · · · · · · · · · · · · · · · · · · | Average DGM Temp: | 28.5 |
| | | | Average DGM Δ H: | 1.8 |

| Train B | | | |
|-----------|--|--|--|
| i i ann 😡 | | | |

7,000.

| ITAILD | 1 | 6 |
|----------------------|-------------|---------------|
| Tube Identification: | OLCOZSHB | Spiked Yes/No |
| Spike Concentration | separate ng | |
| | | |

Measuring Device MII Control Module 🧲 <u>COE 200</u> E

| Clock | Dry Gas | Meter Ter | mperature | Meter | Pump |
|-------------------|--------------------|----------------------|-----------------|-------------------|--------------|
| Time | Meter | Outlet AVG | Inlet | Pressure | Vacuum |
| | | °Č | °C | Δ Η | "Hg Gauge |
| 0 | 84.U | 25 | | 1,4 | 2 |
| 5 | 49.0 | 26 | | 1.4 | 6 |
| 10 | 03.95 | 76 | | 1.01 | S |
| 15 | 98.7 | 27 | | 1.4 | 9 |
| 20 | 103.5 | 28 | | 7,4 | 4 |
| 25 | 104.5 | 28 | | 1.4 | 9 |
| 30 | 113.5 | 25 | | 1.9 | 91 |
| 35 | 1195.5 | 29 | | 1.9 | 9 |
| 40 | 123.0 | 29 | | 1.4 | 9 |
| 45 | 128.4 | 30 | | 14 | 9 |
| 50 | 133.4 | 20 | | 1.9 | 9 |
| 55 | 1978.4 | 3(| 관리가 가장할 것 가 가슴? | 1.4 | 9 |
| 60 | 145.15 | 31 | 민사가 가려봐? 나이야? | 1.9 | <u> </u> |
| tart Time: 4 2 | | Initial Leak Check 🗸 | 01 Lpm@ 19 "Hg | DGMCF: | |
| inish Time: 1/1 < | $\left\{ \right\}$ | Final Leak Check 🖉 | Lpm@ 15"Hg | Sample Volume: | n 15 |
| | | | ~··· · · / · · | Average DGM Temp: | 28.4 |
| Dperator: | ni | 4 | | Average DGM Δ H: | 1.4 |

| Plant: | Clean Habors |] | | Test location: | Stack Breeching |
|---|---|--|--------------------------|--|--|
| Plant Location: | Corunna, Ontario | | | Date: Trucy | 20 246 |
| Test No.: | 7_ | | | Project No.: | 1701 |
| | | 1 | | | |
| | | | | Measuring Device | MII |
| Frain A | a Alexandra de la compañía de la com | | | Control Module 🥣 | 10117 |
| Tube Identification: | 0LC 02549 | Spiked Yes No | | Barometer | EN CAN |
| Spike Concentration | ng | | | | -973 4 4 |
| | | | | Barometric Pressure | |
| Clock | Dry Gas | Meter Ten | | Meter | Pump |
| Time | Meter | Outlet | Inlet | Pressure | Vacuum |
| | | AUG | °C | Δ H H ₂ O | "Hg Gauge |
| 0 | 1697 | 29 | | 20 | |
| 5 | 187 | 20 | <u> </u> | 7.0 | 2 |
| 10 | 144 | 31 | | 7.0 | $ \mathcal{B} -$ |
| | 24.5 | 24 | | + | ⊢–¥, |
| 20 | - 33-5 | 37 | | + 5% | $+\mathcal{E}^{-}$ |
| 25 | - 364 | 33 | | 7.0 | |
| 30 | | 33 | | 2.0 | |
| 30 | | 33 | | + | |
| <u> </u> | | 33 | | + 6.4 | |
| | - 59, | | | 2.0 | <u> </u> |
| 45 | -64.J- | 33 | | + 20 | - 2- |
| 50 | - 69.9- | 23 | | 2.0 | <u> </u> |
| 55 60 | | | | 4.4 | <u> </u> |
| | 1700 | 52 | | <u> </u> | 1 |
| Start Time: | | | | | |
| | 1106 | Initial Leak Check 🖉 | | DGMCF: | 0.991 |
| | 1206 | Initial Leak Check Z | | Sample Volume: | 0.991 |
| | 1206 | | | Sample Volume: Average DGM Temp: | 0.991 |
| | 1206 | | | Sample Volume: | 0.991 51.68 32.2 2.0 |
| Finish Time: | 1206 | | | Sample Volume: Average DGM Temp: | 0.991 57.68 32.2 2.0 |
| Finish Time: | 1206 1206 | Final Leak Check 🦾 | | Sample Volume: Average DGM Temp: Average DGM Δ H: | 32.2 |
| Finish Time: / Train B Tube Identification: | 010013396 | Final Leak Check 🦲 | | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device | 32.2 2.0 |
| Finish Time: / Train B Tube Identification: | | Final Leak Check 🦲 | | Sample Volume: Average DGM Temp: Average DGM Δ H: | 32.2 |
| Finish Time: / Train B Tube Identification: Spike Concentration Clock | Dry Gas | Final Leak Check 🦲 | 2 Lpm@ 75"Hg | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device | 32.2 2.0 |
| Finish Time: , Train B Tube Identification: Spike Concentration | 250 ng | Final Leak Check 🥧 | 2 Lpm@ 75"Hg | Sample Volume: Average DGM Temp: Average DGM ∆ H: Measuring Device Control Module 5 | 32.2. 2.0 MII <i>CoE2.0019</i> Pump Vacuum |
| Finish Time: , Frain B Fube Identification: Spike Concentration Clock | Dry Gas Meter | Final Leak Check 2 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H | 32.2 2.0 MII <i>CoE2.0019</i> Pump Vacuum "Hg |
| Finish Time: / Frain B Tube Identification: Spike Concentration Clock Time | Dry Gas Meter L | Final Leak Check 2 | A Lpm@ 15"Hg | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H ¨H ₂ U | 32.2 2.0 MII <i>CoE2.0019</i> Pump Vacuum |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check 2 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H | 32.2 2.0 MII <i>CoE2.0019</i> Pump Vacuum "Hg |
| Finish Time: | Dry Gas Meter L | Final Leak Check 2 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module \leq Meter Pressure Δ H \Box H ₂ O 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 | 32.2 2.0 MII COE2 DO 19 Vacuum "Hg Gauge |
| Finish Time: / Train B Tube Identification: Spike Concentration Clock Time 0 5 10 | Dry Gas Meter L 47.32 | Final Leak Check Co Spiked (Ye) No Meter Ter Auc- Z 9 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H ¨H ₂ U | 32.2 2.0 MII COE2 DO 19 Vacuum "Hg Gauge |
| Finish Time: , Frain B Fube Identification: Spike Concentration Clock Time 0 5 10 15 | Dry Gas Meter L 47.32 | Final Leak Check Co Spiked (Ye) No Meter Ter Auc- Z 9 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module \leq Meter Pressure Δ H \Box H ₂ O 1.9 1.9 1.9 1.9 1.9 1.9 1.9 1.9 | 32.2 2.0 MII COE2 DO 19 Vacuum "Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check Co Spiked (Ye) No Meter Ter Auc- Z 9 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module \leq Meter Pressure Δ H H H_2 U I . \mathcal{U} | 32.2 2.0 MII COE2.0019 Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: / | Dry Gas Meter L 47.32 | Final Leak Check Co Spiked (Ye) No Meter Ter Auc- Z 9 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module \leq Meter Pressure Δ H H H_2 U I . \mathcal{U} I . \mathcal{U} I . \mathcal{U} | 32.2 2.0 MII COE2.0019 Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check Co Spiked (Ye) No Meter Ter Auc- Z 9 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H ¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬¬ | 32.2 2.0 MII COE2.0019 Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check 2 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H "H ₂ O I. 4 I. 4 | 32.2 2.0 MII COE2.0019 Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check 2 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H "H ₂ O I. 4 I. 4 | 32.2 2.0 MII COE2DO19 Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check 2 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H "H ₂ O I. 4 I. 4 | 32.2 2.0 MII COE2.0019 Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check 2 | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H "H ₂ O I. 4 I. 4 | 32.2 2.0 MII COE2 AO 19 Pump Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check Control Contr | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H "H ₂ O I. 4 I. 4 | 32.2 Z.O MII COEZOOIS Pump Vacuum "Hg Gauge U H Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check Control Contr | nperature Inlet | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H "H ₂ O I. 4 I. 4 | 32.2 2.0 MII COE2 AO 19 Pump Vacuum "Hg Gauge U Hg Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check Control Contr | nperature Inlet °C | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module \leq Meter Pressure Δ H \Box | NII COEZ DO 19 Pump Vacuum "Hg Gauge U H H Gauge |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check C | nperature Inlet °C | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module S Meter Pressure Δ H "H ₂ U I.4 I.4 I.4 I.4 I.4 I.4 I.4 I.4 | NII COEZ DO 19 Pump Vacuum "Hg Gauge U H H H Gauge U H H G Gauge U H H G Gauge U H H G Gauge U H H H G Gauge U H H G Gauge U H H G H H H H H H H H H H H G H H H H |
| Finish Time: | Dry Gas Meter L 47.32 | Final Leak Check Control Contr | nperature Inlet °C | Sample Volume: Average DGM Temp: Average DGM Δ H: Measuring Device Control Module \leq Meter Pressure Δ H \Box | S2.2 Z.O MII COE2A019 Vacuum "Hg Gauge U Vacuum "Hg Gauge U Vacuum "Hg Gauge U Vacuum "Hg Gauge |

| Plant: | Clean Habors | | |
|-----------------|------------------|--|--|
| Plant Location: | Corunna, Ontario | | |
| Test No.: | 2 | | |

| Train A | |
|---------------------------|---------------|
| Tube Identification: 0439 | Spiked Yes No |
| Spike Concentration 500 | ng |
| | |

| Test location: | Stack Breeching | | | |
|----------------|-----------------|--|--|--|
| Date: Tur | 4 20 2016 | | | |
| Project No.: | 21701 | | | |
| | | | | |

| Measuring Device | MI |
|------------------|---------|
| Control Module | 1010 |
| Barometer | ENV.CAN |

Barometric Pressure

29.60

| Clock | Dry Gas | Meter Ten | nperature | Meter | Pump |
|------------|----------------------|-------------|---|------------------------|------|
| Time Meter | -Outlet AVC °C | Inlet °C | Pressure Δ Η Η ₂ υ | Vacuum "Hg Gauge | |
| 0 | 80.95 | 31 | A | 2.0 | 5 |
| 5 | 85.5 | 33 | 1 | 2.0 | 57 |
| 10 | 90.6 | 33 | | 2.0 | 4 |
| 15 | 95.5 | 33 | a de la constante de la constante de la | 2.0 | \$ |
| 20 | 180.C | 33 | | 20 | 9 |
| 25 | 105.U | 34 | | 2.0 | 9 |
| 30 | 110,9 | 34 | | 2.0 | 9 |
| 35 | 115.2 | 34 | | 2.0 | Ś |
| 40 | 120.7 | 34 | | 2.0 | 9 |
| 45 | 125.2 | 34 | | 2.0 | 9 |
| 50 | 130.0 | 34 | | 7.0 | 9 |
| 55 | 134.0 | 34 | | 20 | 9 |
| 60 | 139,51 | 34 | | 20 | |
| | | | | | |

| Finish Time: 132.(Final Leak Check (_,0/Lpm@/5"Hg Sample Volume: Average DGM Temp: 33.5 | |
|--|---|
| Average DGM Temp: 33 S | 3 |
| | |
| Average DGM Δ H: 2.0 | |

| | in | |
|--|----|--|
| | | |
| | | |

| 3 (ani u | and the second | | | |
|----------------------|--|---------|-----------|--|
| Tube Identification: | OLC025429 | Spiked | Yes (No) | |
| Spike Concentration | ng | | | |
| | ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ | Teles (| | |
| | | | · | |

Measuring DeviceMIIControl ModuleCoE 2001 %

| Clock | Dry Gas | Meter Te | emperature | Meter | Pump |
|-------------|---|---------------------|--------------|-------------------------------------|------------------------|
| Time | Meter | Quiler AVC °C | Inlet °C | Pressure Δ Η τ ₂ Ο | Vacuum "Hg Gauge |
| 0 | 13.68 | 34 | | 1.4 | Y |
| 5 | 19.9 | 34 | | 1.4 | 1 |
| 10 | 82.7 | 34 | | nG | 9 |
| 15 | 139.9 | 34 | | 1.4 | 4 |
| 20 | 2410 | 35 | | 1.9 | 9 |
| 25 | 79.0 | 35 | | 1.4 | 9 |
| 30 | 144.2 | 35 | | 1.4 | 4 |
| 35 | 49.3 | 35. | | 1.4 | 9 |
| 40 | 54.3 | 35 | | 1.4 | 4 |
| 45 | 59,5 | 35 | | 1.4 | 9 |
| 50 | 64.6 | 35 | | 1.4 | 9 |
| 55 | 69:40 | 35 | | 1.4 | I I |
| 60 | 174,78 | 135 | | 1.4 | |
| | | | | | 0001 |
| | art Time: 1221 Initial Leak Check 40(Lpm@ /5 "Hg | | DGMCF: | 0.996 | |
| inish Time: | 1321 | Final Leak Check | CA Lpm@ 5"Hg | Sample Volume: Average DGM Temp: | 61.10 |
| Operator: | | | | Average DGM Δ H: | 1.4 |
| Julianon. | | 1 | | Average DONIATI. | 11 A 4 1 |

Spiked

A

ng

Yes No

| Plant: | Clean Habors |
|-----------------|------------------|
| Plant Location: | Corunna, Ontario |
| Test No.: | U U |

Ø

Train A

7

Tube Identification:

Spike Concentration

| Test location: | Stack Breeching |
|------------------|-----------------|
| Date: | 4 20 2016 |
| Project No.: | 21701 |
| | |
| Measuring Device | MII |
| Control Module | 1017 |
| Barometer | FAILORA |

Barometric Pressure

29

| Clock | Dry Gas | Meter Tem | perature | Meter | Pump |
|--|------------|----------------------|-------------|-------------------------------------|------------------------|
| Time | Meter L | Outlet AVG- °C | Inlet °C | Pressure Δ Η Η ₂ Ο | Vacuum "Hg Gauge |
| 0 | 46.32 | 31 | 8 | 20 | 4 |
| 5 | 3.5 | 32 | | 7.0 | É |
| 10 | 56.4 | 37 | l | 7.0 | -7 |
| seistevitei <mark>15</mark> der hitteris i | 39,1 | 32 | | 2.0 | 5 |
| 20 | | 32 | | 2.0 | 9 |
| 25 | 6A.0 | 34 | | 20 | B |
| 30 | 12.0 | 34 | | 7.0 | F |
| 35 | 14.9 | 35 | | 20 | G |
| 40 | 3410 | 33 | | 7.0 | 4 |
| 45 | 89.7 | 35 | | 2.0 | B |
| 50 | 94.4 | 3534 | | 7.0 | B |
| 55 | 99.5 | 3434 | | 2.0 | 45 |
| 60 | 104,80 | 338-24 | | 20 | 4 |

| Start Time: 133% | Initial Leak Check 2.01 Lpm@ 15"Hg | DGMCF: 0.991 |
|-------------------|------------------------------------|------------------------|
| Finish Time: 1424 | Final Leak Check Lor Lpm@ 16"Hg | Sample Volume: 58.4% |
| | | Average DGM Temp: 33.4 |
| | | Average DGM Δ H: 2.0 |

| | Train B | |
|--|-----------|-----------|
| 1. | Tube Ider | ntificati |
| | Spike Con | |
| - 1 | | |

| rain B | | | 4.6 | A | |
|---------------------|---------|----|--------|-------|----|
| ube Identification: | a 33699 | Y | Spiked | Xes) | No |
| oike Concentration | 400' | ng | | | |

Measuring Device **Control Module**

MII かんてつつ ñ

| Clock | Dry Gas | Meter Te | emperature | Meter | Pump |
|-------------------|-------------|----------------------------------|-----------------------|--------------------------------------|---------------------------------------|
| Time | Meter | Quiter AVC- C | inlet °C | Pressure Δ Η ¨H ₂ Ο | Vacuum "Hg Gauge |
| 0 | 83.17 | 33 | | 1.9 | 4 |
| 5 | 88.Y | 37 | | 1.4 | 6 |
| 10 | 93.4 | 33 | 이 문화가 가슴을 물건하는 것이 같아. | 1.4 | E |
| 15 | 99.13 | 33 | | 1.9 | Z. |
| 20 | 163.0 | -33 | | 14 | 8 |
| 25 | 107.5 | 33 | | 14 | 45 |
| 30 | 12,4 | 33 | | 1.4 | S |
| 35 | 117.2 | 39 | | 1.4 | 4 |
| 40 | 122.4 | 34 | | 1.4 | 8 |
| 45 | 127.2 | 34 | | 1.6 | 4 |
| 50 | 1322 | 34 | | TR4 | 3 |
| 55 | 132.2 | 34 | | 11.4 | 4 |
| 60 | 142.00 | 34 | | 14 | 4 |
| | | | | | · · · · · · · · · · · · · · · · · · · |
| Start Time: 1338 | | Initial Leak Check | D(Lpm@ S"Hg | DGMCF: | 2.496 |
| Finish Time: 1426 | | Final Leak Check 🥿 | O Lpm@ /6"Hg | | |
| | KAIN- | | | Average DGM Temp: | <u> 33,5 </u> |
| Operator: | i 2 de Vite | Construction Company and Company | | Average DGM Δ H: | 1.4 |

| | | ORTECH Envir Mercury Tube I | | | | |
|---------------------------------|--|--------------------------------|---|-----------------------------|-----------------------|--|
| Plant: | Clean Habors | ····· # | • • • • · · · · · | Test location: | Stack Breeching | |
| Plant Location: | Corunna, Ontario | | | Date: July | · 20 7016 | |
| Test No.: | 5 | | | Project No.: | 2010 | |
| | | | | | | |
| | | | | Measuring Device | MI | |
| Train A | al | Cultural Alexandre | | Control Module Barometer | 1011 | |
| Tube Identification: | and the second | Spiked (Yes No | | | IBN:CAN | |
| Spike Concentration | 1400 ng | | | Barometric Pressure | 79 <1 | |
| | | | | Duromentorio | 6.2 | |
| Clock | Dry Gas | Meter Tem | perature | Meter | Pump | |
| Time | Meter | Outlet | Inlet | Pressure | Vacuum | |
| | | AVG | | ΔH | "Hg | |
| | | °C | °C | H₂U | Gauge | |
| 0 | 5.3 | 32 | | 20 | 4 | |
| 5 | 10.7 | 34 | | 2.0 | <u> </u> | |
| 10 | 155 | 35 | | 20 | <u> </u> | |
| 15 (15) | 70.4 | 30 | ga) a constant grant sea | 2,0 | <u> </u> | |
| 20 | 25.3 | 30 | | 7.0 | 9 | |
| 25 | 30.2 | 37 | dina kaominina dia Managambana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana Ny faritr'o dia Managambana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin'ny fisiana amin | 20 | 6 | |
| 30 | 35.1 | 37 | | 20 | <u> </u> | |
| 35 | 40.0 | 37 | | 2.0 | <u> </u> | |
| 40 | 45.0 | 37 | | 20 | <u> </u> | |
| 45 | 50.0 | 2 | | 20 | 4 | |
| 50 | 54.7 | 37 | | 7.0 | 6 | |
| 55 | 3471 | 31 | | 20 | 6 | |
| 60 | 14.46 | 3 | a maggag <mark>i</mark> sasa | 120 | $\underline{}$ | |
| | 22 | | 1 1 | DGMCF: | 0091 | |
| Start Time: / Finish Time: / | 434 | Initial Leak Check | | Sample Volume: | <u>0.991</u> 58.65 | |
| | 227 | That Leak Check Col | M chuice 16 11P | Average DGM Temp: 36. | | |
| | | | | Average DGM Δ H: | 2/1 | |
| | 영상 영상 영상 영상 영상 영상 | 이 이 아파 바라 옷을 받으며? | in de la seconda de la sec Na seconda de la seconda de | | | |
| Train B | | | | | | |
| Tube Identification: | 0LC 025470 | Spiked Yes No | | Measuring Device | MI | |
| Spike Concentration | ng | | | Control Module | COE 20019 | |
| | | | | | | |
| Clock | Dry Gas | Meter Ten | and the second se | Meter | Pump | |
| Time | Meter | Qutlet | Inlet | Pressure | Vacuum | |
| | | 40- | °C | Δ H H ₂ O | "Hg | |
| | | | Ç | | Gauge | |
| 0 | 45.12 | 34 | 1 | 1.4 | - ak- | |
| 5 | 45.5 | 34 | | 1.4 | +-3 | |
| 10 | <u> </u> | 34 | | 1.4 | 1-70- | |
| 15 | 157.5 | 35 | | 1.4 | | |
| 20 | 164.5 | 35 | | <u> 44.</u> | <u> </u> | |
| 25 | 695 | 35 | | 14 | | |
| 30 | +74.3 | 37 | 1 | 19 | 1-2 | |
| 35 | 179.9 | 36 | | 14 | <u> </u> | |
| 40 | 19515 | 37 | | 1-9 | +2 | |
| 45 | 170.6 | 32 | | 1.4 | | |
| 50 | 196.2 | 34 | | 1-1-9 | <u> </u> | |
| 55 | 101.4 | 31 | 1 | 1-4 | | |
| 60 | | 37 | | | 4 | |

| 45 | 40.6 | 27 | | 1.4 | 4 |
|--------------|--------|--------------------------|-----------|---------------------------------------|-------|
| 50 | 196.7 | 37 | | 1.9 | 9 |
| 55 | 101.0 | 31 | | 1.4 | 9 |
| 60 | 106.09 | | | 1.9 | 4 |
| | | | J | | |
| Start Time: | 1454 | | m@ 🏠 "Hg | DGMCF: | 0.996 |
| Finish Time: | 1554 | Final Leak Check 6.01 Lp | m@ [6 "Hg | Sample Volume: | 63.57 |
| | | | | | |
| | | | | Average DGM Temp: | 35.4 |
| Operator: | OHUS | | | Average DGM Temp: Average DGM Δ H: | 35.8 |

| Plant: | Clean Habors | |
|-----------------|------------------|--|
| Plant Location: | Corunna, Ontario | |
| Test No.: | 0 | |
| | | |
| Train A | | |

| Irain A | | | | <u> </u> |
|----------------------|--|----|--------|----------|
| Tube Identification: | OLCOZSYTH | | Spiked | Yes No |
| Spike Concentration | Cardina and Cardina an | ng | | |
| | | | | |

Test location:Stack BreechingDate:July 20 2016Project No.:21701

| Measuring Device | MI |
|------------------|---------|
| Control Module | 1010 |
| Barometer | FNV-CAN |
| | |

Barometric Pressure

55

| Clock | Dry Gas | Meter Ter | nperature | Meter | Pump |
|-------------------------|--|----------------------|----------------|-------------------|------------|
| Time | Meter | Outlet | Inlet | Pressure | Vacuum |
| | | AR | | ΔH | "Hg |
| | L | °C | °C | "H ₂ U | Gauge |
| 0 | 105.86 | 35 | | 2.0 | Gif |
| 5 | 70.6 | 36 | | 20 | 1 |
| 10 | Fig | 36 | | 7.0 | <u> </u> |
| 15 | 90.4 | 36 | | 2.0 | <u>q</u> . |
| 20 | 85.3 | 36 | | 2.0 | <u> </u> |
| 25 | 90.4 | 36 | | 2.5 | <u> </u> |
| 30 | 953 | 36 | | 2.0 | <u> </u> |
| 35 | 100.4 | 36 | | 2.0 | <u> </u> |
| 40 | 105.6 | マコ | | 2.0 | 9 |
| 45 | 110.7 | 37 | | 20 | <u> </u> |
| 50 | 115.8 | 37 | | 2.0 | <u> </u> |
| 55 | 20.4 | 37 | | 20 | <u></u> |
| 60 | 123.91 | 31 | | 20 | <u> </u> |
| o ne ne de agrèce de la | | | | | (|
| tart Time: 160 | 2 | Initial Leak Check 🧹 | 0(Lpm@ / 6"Hg | DGMCF: | 0.991 |
| inish Time: 170 | e la | Final Leak Check | O(Lpm@KSHg | Sample Volume: | <u></u> |
| | | | | Average DGM Temp: | 36.5 |
| | | | | Average DGM Δ H: | Z.0 |

| Train B | | | 5 | ł |
|----------------------|----------|--------|-----|----|
| Tube Identification: | OL331414 | Spiked | Yes | No |
| Spike Concentration | 7600 n | g | | |
| Spine concentration | | 의 | | |

Operator:

6

Measuring Device MII Control Module COE 200 1.9

Average DGM Temp:

Average DGM Δ H:

| Dry Gas | Meter Tem | iperature | Meter | Pump |
|----------|---|---|--|--|
| Meter | Outlet | Inlet | Pressure | Vacuum |
| | 4 4 44 | | ΔH | "Hg |
| LE L | °C | °C | "H ₂ U | Gauge |
| 8.50 | 36 | 1 | 1.9 | H |
| 14.0 | 36 | | 1.0 | 6 |
| 18:7 | 36 | | 1.4 | |
| 25.0 | 36 | te de la facte de la terre de | 1.4 | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ |
| 30.0 | 37 | | 1.4 | |
| 35.5 | 37 | | 1.4 | 9 |
| 40.0 | 37 | | 1.4 | 3 |
| US.S | 31 | | i.y | |
| 50.0 | 27 | | 1.0 | |
| 65.9 | 39 | | 1.0 | 4 |
| 61.2 | 38 | | 14 | <u> </u> |
| 76.3 | 23 | | <u> </u> | <u> </u> |
| 1-71.73 | 38 | e e la constant de la constant Referencia de la constant de la cons | <u>1 [4</u>] | 4 |
| <u>~</u> | Initial Leak Check | 1 Lpm@/(, "Hg | DGMCF: | 0.996 |
| ňe | Final Leak Check | 1 Lpm@ /45"Hg | Sample Volume: | 63.23 |
| | Meter 25 L 9.50 14.0 15:7 25:0 30:0 35:5 | Meter Outlet 1 2 3.50 3.6 14.0 3.6 13.7 3.6 30.0 3.7 35.5 3.7 40.0 3.6 35.5 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.7 50.0 3.8 60.3 3.8 71.3 3.8 71.3 3.8 | Meter Outlet Inlet 1 1 °C °C 1 2 3 1 1 1 3 1 1 3 3 1 1 3 3 1 1 3 3 1 1 3 3 1 1 3 3 1 1 1 3 3 1 1 1 3 3 1 1 3 1 3 1 1 3 1 1 1 1 3 1 1 1 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | Meter Outlet- Hul- °C Inlet Pressure A H "H ₂ U 9.50 36 °C 34 14.0 36 144 12.7 36 144 12.7 36 144 12.7 36 144 12.7 36 144 12.7 36 144 12.7 36 144 12.7 36 144 25.0 37 144 30.0 37 144 30.0 37 144 30.0 37 144 30.0 37 144 30.0 37 144 30.0 37 144 30.0 37 144 40.0 37 144 56.9 36 144 66.3 343 144 71.73 38 144 71.73 343 144 |

3



APPENDIX 3

ORTECH Equipment Calibration Data (4 pages) **ORTECH Environmental** Dry Gas]

| 03-J004 | Vost 2 | July 22, 2016 | 29.47 | <.011pm @ 21"Hg |
|-----------------------|--------------|---------------|---------------------|-------------------|
| Calibration Procedure | Meter Number | Date | Barometric Pressure | System Leak Check |

ft³ cm * 1.332 litres per cm/28.3168 litres per ft³

| Pbar (in. Hg) | (Pbar in. Hg+DGMPressure/13.6) |
|----------------------|--------------------------------|
| Tdgm °F+460 | Tstd °F+460 |
| Vstd ft ³ | Vdgm ft ³ |
| DGMCF= | |

| | | فللمحتمد والاستعاد والمستقد مستقدان المستراد ومستقدها ويتمام ومسترجعا والارتباع والمرابع فالمنام والمسترجين والمتعرين | MII NUMBERS |
|------------------------|--|---|-------------|
| Meter Calibration Data | | | · · · |

| David Utley | Calibrated By |
|-------------|---------------|
| | |
| COE20028 | Barometer |
| A01463 | Gasometer |
| A10117 | DGM |
| | |

| David Utley | 1 m cl (L cm | anala Nolan | 0 |
|---------------|---------------|--------------------------|---|
| Calibrated By | Signature | Reviewed and Accepted By | |

| | adino | Gasometer | Gasometer Gasometer | DGM | DGM Reading | DGM | | DGM | DGM | DGM | I III C | MOLA |
|-------------|-------|-----------------|-----------------------|---------|-------------|-----------------|-------------|----------------------|--------|-------------|---------|------|
| cm | D | Volume | Volume Temperature | | ر | Volume | Temperature | Pressure | Outlet | Calibration | | Rate |
| Initial | cm | ft ³ | °C | Initial | Final | ft ³ | | in. H ₂ O | °C | Factor | min. | lpm |
| 81.60 52.00 | 29.60 | 29.60 1.392 | 24.0 | 38.300 | 78.790 | 1.430 | 31.0 | 2.0 | 31.0 | 0.992 | 42 | 1.0 |
| 52.00 30.30 | 3 | 21 70 1 1 021 | | 78.790 | 108.400 | 1.046 | 31.0 | 2.0 | 31.0 | 0.994 | 31 | 1:0 |
| 4 3 | | 1.035 | | 8.400 | 38.650 | 1.068 | 31.0 | 2.0 | 31.0 | 0.987 | 31 | 1.0 |

otherwise the meter must be repaired and/or adjusted as necessary and recalibrated prior to use. (Environment Canada Reference Method BPS 1/RM/8, Section 6) If not the calibration must be repeated. Also, the DGMCF average value must be 1.00 ± 0.05 , Acceptance Criteria: Individual values of DGM calibration factor must be within \pm 1.5% of the average value.

DGMCF AVERAGE 0.991 I Lpm

ORTECH Environmental Trendicator Calibration

| Calibration Procedure | 03-J005 |
|--------------------------|---------------|
| Trendicator Type | Nutech |
| MII | A10117 |
| Date | July 22, 2016 |
| Calibrated By | David Utley |
| Signature | Didle |
| Reviewed and Accepted By | angla malan |

| Fluke Calibrator Output | Tredicator D | isplay Value | Percent Difference |
|-------------------------|-------------------|------------------|-----------------------|
| (COE 20024) | Before Adjustment | After Adjustment | 1 |
| (°C) | (°C) | (°C) | (%) |
| 0 | 0 | JA | 0.0 |
| 10 | 10 | | 0.0 |
| 20 | 20 | | 0.0 |
| 50 | 50 | | 0.0 |
| 75 | 75 | | 0.0 |
| 100 | 100 | | 0.0 |
| 125 | 124 | | 0.8 |
| 150 | 149 | | 0.7 |
| 200 | 200 | | 0.0 |
| 300 | 300 | | 0.0 |
| 400 | 400 | | 0.0 |
| 500 | 500 | | 0.0 |
| 600 | 600 | V | 0.0 |

% Difference = (micromite - after adjustment reading)x 100 micromite

Acceptance Criteria:

Trendicator display must read within $\pm 1.5\%$ of the micromite value at each output. Otherwise, the Trendicator must be repaired and/or adjusted as necessary, and recalibrated prior to use. (MOE Source Testing Code, Version #2, Method 5)

ORTECH Environmental

ORTECH Environmental Dry Gas Meter Calibration Data

| Calibration Procedure 03-J004 Meter Number Vost 5 | Jul | Barometric Pressure |
|--|-----|---------------------|
|--|-----|---------------------|

 $ft^3 = cm^* 1.332$ litres per cm/28.3168 litres per ft^3

| Pbar (in. Hg) | (Pbar in. Hg+DGMPressure/13.6) |
|----------------------|--------------------------------|
| Tdgm °F+460 | Tstd [°] F+460 |
| Vstd ft ³ | Vdgm ft ³ |
| DGMCF= | |

| MII NUMBERS | COE 20018 | A01463 | COE 20028 | |
|-------------|-----------|-----------|-----------|--|
| N IIW | DGM | Gasometer | Barometer | |

| David Utley | 1 7 2018 | ted By CANON's MG | |
|---------------|-----------|--------------------------|--|
| Calibrated By | Signature | Reviewed and Accepted By | |

| Carbonicer Nearing cm Comment cm Temperature ft ³ L Volume Temperature ft ³ Initial Final Final ft ³ °C Initial ft ³ °C 80.80 66.20 14.60 0.687 23:0 83.41 103.24 0.700 26.0 66.20 51.70 14.50 0.682 24.0 3.24 22.61 0.684 27.0 51.70 36.50 0.715 24.0 22.61 43.13 0.725 28.0 | DGM Reading | | 5 | | DGM Time | |
|---|----------------------|---|----------------------|----|-------------|------|
| °C Initial Final ft ³ 23.0 83.41 103.24 0.700 24.0 3.24 22.61 0.684 24.0 22.61 0.725 | | | 1. E | | Calibration | Rate |
| 23:0 83:41 103.24 0.700 24.0 3.24 22.61 0.684 24.0 22.61 43.13 0.725 | C Initial Final | | in. H ₂ O | °C | Factor min. | |
| 23:0 83.41 103.24 0.700 24.0 3.24 22.61 0.684 24.0 22.61 43.13 0.725 | | | L | ┝ | | |
| 24.0 3.24 22.61 0.684 24.0 2.2.61 43.13 0.725 | 23.0 83.41 103.24 | | 1.4 | _ | 0.987 20 | |
| 24.0 3.24 22.61 0.684 24.0 22.61 43.13 0.725 | | | - | | | |
| 24.0 22.61 43.13 0.725 | 24.0 3.24 22.61 | | 4. | _ | 1.004 1.004 | |
| 0.715 | | | _ | | C | 10 |
| | 24.0 22.61 43.13 | 2 | 1.4 | | 0.770 | |
| | | and the second se | | | | |

Acceptance Criteria:

Individual values of DGM calibration factor must be within $\pm 1.5\%$ of the average value. If not the calibration must be repeated. Also, the DGMCF average value must be 1.00 ± 0.05 , otherwise the meter must be repaired and/or adjusted as necessary and recalibrated prior to use. (Environment Canada Reference Method EPS 1/RM/8, Section 6)

0.996

lLpm

DGMCF AVERAGE

Revision June 5, 2007

ORTECH Environmental Trendicator Calibration

| Calibration Procedure | 03-J005 |
|------------------------------|---------------|
| Trendicator Type | Jenco 765 |
| MII | COE 20018 |
| Date | July 22, 2016 |
| Calibrated By | David Utley |
| Signature | Dillo |
| Reviewed and Accepted By | MAROLA NORM |

| Fluke Calibrator Output | Tredicator D | isplay Value | Percent Difference |
|-------------------------|-------------------|------------------|-----------------------|
| (COE 20024) | Before Adjustment | After Adjustment | |
| (°C) | (°C) | (°C) | (%) |
| 0 | 0 | JA | 0.0 |
| 10 | 10 | | 0.0 |
| 20 | 20 | | 0.0 |
| 50 | 50 | | 0.0 |
| 75 | 75 | | 0.0 |
| 100 | 100 | | 0.0 |
| 125 | 125 | | 0.0 |
| 150 | 150 | | 0.0 |
| 200 | 199 | | 0.5 |
| 300 | 300 | | 0.0 |
| 400 | 400 | | 0.0 |
| 500 | 500 | | 0.0 |
| 600 | 600 | | 0.0 |

% Difference = (<u>micromite - after adjustment reading</u>)x 100 micromite

Acceptance Criteria:

Trendicator display must read within $\pm 1.5\%$ of the micromite value at each output. Otherwise, the Trendicator must be repaired and/or adjusted as necessary, and recalibrated prior to use. (MOE Source Testing Code, Version #2, Method 5)

ORTECH Environmental



APPENDIX 4

Mercury Analytical Report (1 page)

Sorbent Trap Analysis Report

Project Number: 2007498

Turn-around: Standard

Plant:ORTECH EnvironmentalContact:David UtleyPhone:(905)-822-4120*235Email:dutley@ortech.ca

Date:01/08/2016Analyst(s):Patrick CookMethod:EPA 7473Method Uncertainty:± 10%

| Trap ID | AGS Mass (ng) | Section 1 Mass (ng) | Section 2 Mass (ng) | Total Mass (ng) | Section 3 Mass (ng) | Spike Level (ng) | Brea | (%) Spike Recovery | Source | Notes |
|-----------|---------------|---------------------|------------------------|-----------------|------------------------|------------------|-------|-----------------------|--------|-------|
| 01369249 | | 184.2 | 0.2 | 184.4 | | 100 | 0.11% | | | |
| OLC025413 | | 93.9 | 0.0 | 93.9 | | | 0.00% | | | |
| OLC025459 | | 91.4 | 1.0 | 92.4 | | | 1.14% | | | |
| OLC013396 | | 332.4 | 1.3 | 333.7 | | 250 | 0.40% | | | |
| 01291911 | | 563.7 | 1.3 | 565.0 | | 500 | 0.23% | | | |
| OLC025428 | | 86.7 | 0.0 | 86.7 | | | 0.00% | | | |
| OLC025473 | | 76.3 | 0.0 | 76.3 | | | 0.00% | | | |
| OL336499 | | 880.5 | 0.0 | 880.5 | | 800 | 0.00% | | | |
| OL335287 | | 1503 | 0:0 | 1503 | | 1400 | 0.00% | | | |
| OLC025470 | | 96.5 | 0.0 | 96.5 | | | 0.00% | | | |
| OLC025479 | | 96.0 | 0.8 | 96.8 | | | 0.85% | | | |
| OL331414 | | 2668 | 1.3 | 2669 | | 2600 | 0.05% | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | | | | | | |

MDL = 0.493 ng LOQ = 10 ng

OHIGAMEX

Ohio Lumex Co., Inc. 30350 Bruce Industrial Pkwy, Solon, OH 44139 | Phone: (330)405-0837 | Fax: (330) 405-0847



APPENDIX 5

Clean Harbors Process Data (12 pages)

| TEST 1 | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SDA . | Stack |
|---|--|-----------|----------------|----------|----------------|----------|----------------|----------|---|--|--------------------------------------|--|--|-------------------------|------------|-----------|
| | | LPM | LPM | LPM | | | SCFM | LPM | | | | | | | | Degrees C |
| Date | Time | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | NAMES OF TAXABLE PARTY OF TAXABLE PARTY | Construction of the owner | and an a second second second second | Contraction of the International Contractional Contra | TE-241 | TE-203 | TE-204 | TE-258 |
| 7/20/2016 | 9:51:00 | 28.395 | 9.465 | 168.9075 | 161.685 | 4.69 | 281.4 | 14.4375 | 22670.21 | 9966.332 | 87646 | 1375.5 | 993.2 | 481.4 | 187.5 | 189.1 |
| 7/20/2016 | 9:52:00 | 28.185 | 9.735 | 168.6712 | 162.585 | 4.31 | 258.6 | 13.425 | 23112.61 | 10067.46 | 88495 | 1370.375 | 989.3 | 483.2 | 187.5 | 189.1 |
| 7/20/2016 | 9:53:00 | 28.32 | 9.965 | 168.5363 | 163.44 | 4.3075 | 258.45 | 14.5125 | 22939.8 | 9960.714 | 88348 | 1370.75 | 989.7 | 482.6 | 188 | 189.1 |
| 7/20/2016 | 9:54:00 | 28.29 | 9.795 | 168.9075 | 162.27 | 4.2775 | 256.65 | 14.5125 | 22932.89 | 10179.82 | 88262 | 1366.25 | 992.1 | 484 | 188 | 189.1 |
| 7/20/2016 | 9:55:00 | 28.485 | 9.675 | 167.9175 | 162.9 | 4.31375 | 258.825 | 14.5125 | 22760.08 | 10044.98 | 87699 | 1369 | 992.5 | 483.2 | 188 | 189.1 |
| 7/20/2016 | 9:56:00 | 28.395 | 9.68 | 169.6162 | 163.035 | 4.3175 | 259.05 | 14.5125 | 22849.94 | 10162.96 | 89239 | 1367.625 | 990.9 | 483.6 | 188 | 189.1 |
| 7/20/2016 | 9:57:00 | 28.545 | 9.78 | 168.2438 | 163.035 | 4.315 | 258.9 | 14.5125 | 22497.4 | 10022.51 | 87501 | 1373.875 | 991.7 | 483 | 188 | 189.1 |
| 7/20/2016 | 9:58:00 | 28.35 | 9.595 | 168.8175 | 162.585 | 4.31625 | 258.975 | 14.5125 | 22670.21 | 10022.51 | 87903 | 1374.25 | 991.5 | 483.5 | 188 | 189.1 |
| 7/20/2016 | 9:59:00 | 28.23 | 9.91 | 168.6263 | 163.8 | 4.68 | 280.8 | 14.5125 | 22670.21 | 10022.51 | 86408 | 1380 | 991.5 | 482.2 | 187.5 | 189.1 |
| 7/20/2016 | 10:00:00 | 28.635 | 9.705 | 169.4812 | 163.845 | 4.31625 | 258.975 | 14.5125 | 22932.89 | 10022.51 | 88983 | 1374 | 992.6 | 483.7 | 188 | 189.1 |
| 7/20/2016 | 10:01:00 | 28.2 | 9.46 | 168.2438 | 163.305 | 4.325 | 259.5 | 14.5125 | 22849.94 | 10022.51 | 87768 | 1377.5 | 992.8 | 483 | 187.5 | 189.1 |
| 7/20/2016 | 10:02:00 | 28.41 | 9.645 | 169.29 | 162.765 | 4.31625 | 258.975 | 14.4375 | 22849.94 | 10050.6 | 88396 | 1372.75 | 995.9 | 484.4 | 188 | 189.1 |
| 7/20/2016 | 10:02:00 | 28.155 | 9.825 | 167.0175 | 161.685 | 4.32125 | 259.275 | 14.4375 | 22670.21 | 9938.242 | 87035 | 1379.75 | 994.5 | 483.7 | 188 | 189.3 |
| 7/20/2016 | 10:04:00 | 28.245 | 9.83 | 168.2438 | 161.1 | 4.29375 | 257.625 | 14.4375 | 22932.89 | 10039.37 | 87829 | 1377.75 | 994.7 | 484.7 | 188 | 189.1 |
| 7/20/2016 | 10:04:00 | 28.335 | 9.545 | 167.2987 | 161.64 | 4.30625 | 258.375 | 14.4375 | 22753.16 | 9927.006 | 92403 | 1377.75 | 994.7 | 484.1 | 188 | 189.1 |
| | 10:05:00 | 28.555 | | 168.3 | 161.775 | 4.50625 | 258.575 | 13.9875 | 22670.21 | 10033.75 | 87698 | 1380.75 | 996.5 | 484.1 | 188.5 | 189.1 |
| 7/20/2016 | | | 9.645 9.435 | 168.3 | | | | | 22753.16 | | | | 996 | 483.6 | 188.5 | 189.1 |
| 7/20/2016 | 10:07:00 | 28.425 | | | 161.775 | 4.33 | 259.8 | 13.9875 | | 9910.152 | 93196 | 1386.625 | | | | |
| 7/20/2016 | 10:08:00 | 28.185 | 9.57 | 168.6712 | 162.54 | 4.3125 | 258.75 | 13.9875 | 22849.94 | 10022.51 | 89757 | 1379.75 | 995.4 | 485.3 | 188.5 | 189.3 |
| 7/20/2016 | 10:09:00 | 28.665 | 9.6 | 166.3537 | 161.235 | 4.3075 | 258.45 | 13.9875 | 23202.47 | 10022.51 | 93561 | 1382.375 | 996.2 | 484.6 | 188.5 | 189.1 |
| 7/20/2016 | 10:10:00 | 28.35 | 9.54 | 169.245 | 162.54 | 4.66875 | 280.125 | 13.9875 | 22932.89 | 10044.98 | 88724 | 1374.875 | 993.6 | 485.6 | 189 | 189. |
| 7/20/2016 | 10:11:00 | 28.185 | 9.615 | 168.7163 | 161.415 | 4.6825 | 280.95 | 13.9875 | 23202.47 | 10044.98 | 95203 | 1380.75 | 995 | 483.7 | 189 | 190. |
| 7/20/2016 | 10:12:00 | 28.065 | 9.3 | 168.345 | 162.54 | 4.3075 | 258.45 | 13.9875 | 22932.89 | 10044.98 | 88556 | 1374.75 | 995.1 | 484.4 | 189 | 190. |
| 7/20/2016 | 10:13:00 | 28.29 | 9.38 | 167.4 | 161.415 | 4.7 | 282 | 13.9875 | 23202.47 | 10044.98 | 93764 | 1384.5 | 995.6 | 482.7 | 189 | 189. |
| 7/20/2016 | 10:14:00 | 28.44 | 9.515 | 168.9525 | 161.37 | 4.31875 | 259.125 | 13.9875 | 22760.08 | 10044.98 | 86535 | 1382.125 | 993.1 | 482.8 | 189 | 189. |
| 7/20/2016 | 10:15:00 | 28.215 | 9.36 | 167.8725 | 160.605 | 4.315 | 258.9 | 13.9875 | 23285.42 | 10067.46 | 93299 | 1385.75 | 993.8 | 481.9 | 188.5 | 190.3 |
| 7/20/2016 | 10:16:00 | 28.305 | 9.835 | 169.5712 | 161.91 | 4.305 | 258.3 | 13.9875 | 22760.08 | 10067.46 | 87936 | 1382.5 | 992.4 | 483.8 | 189 | 189.3 |
| 7/20/2016 | 10:17:00 | 28.005 | 9.505 | 168.5363 | 162.27 | 4.31 | 258.6 | 13.9875 | 23195.56 | 10078.69 | 92146 | 1382 | 994.4 | 483.5 | 189 | 190. |
| 7/20/2016 | 10:18:00 | 28.305 | 9.59 | 169.0087 | 162.9 | 4.31125 | 258.675 | 13.9875 | 22670.21 | 9960.714 | 88463 | 1380.25 | 993.8 | 485.6 | 189.5 | 190. |
| 7/20/2016 | 10:19:00 | 28.305 | 9.69 | 168.9525 | 155.295 | 4.6875 | 281.25 | 13.9875 | 23285.42 | 10084.31 | 92282 | 1381.25 | 992.5 | . 485.6 | 189.5 | 190. |
| 7/20/2016 | 10:20:00 | 28.425 | 9.65 | 168.6263 | 145.8 | 4.69125 | 281.475 | 13.9875 | 22849.94 | 9960.714 | 87641 | 1386.375 | 992.5 | 485.9 | 190 | 190. |
| 7/20/2016 | 10:21:00 | 28.53 | 9.625 | 168.6712 | 144.63 | 4.29625 | 257.775 | 13.9875 | 23202.47 | 10000.04 | 89136 | 1385.5 | 993.4 | 484 | 189.5 | 190. |
| 7/20/2016 | 10:22:00 | 28.2 | 9.58 | 168.48 | 145.215 | 4.675 | 280.5 | 13.9875 | 22587.26 | 10000.04 | 87209 | 1388 | 993.6 | | 189.5 | 190. |
| 7/20/2016 | 10:23:00 | 28.605 | 9.695 | 168.0075 | 143.37 | 4.31 | 258.6 | 13.9875 | 23195.56 | 10028.13 | 89641 | | 993.2 | | 188.5 | 190. |
| 7/20/2016 | 10:24:00 | 28.455 | 9.66 | 169.0087 | 144.675 | 4.3225 | 259.35 | 13.9875 | 22849.94 | 9915.77 | 88559 | 1389.5 | 996.7 | 482.9 | 189 | 190. |
| 7/20/2016 | 10:25:00 | 28.44 | 9.54 | 167.2987 | 143.46 | 4.30875 | 258.525 | 13.9875 | 23382.2 | | 91867 | 1389.25 | 994.5 | | 189 | 190. |
| 7/20/2016 | 10:25:00 | 28.38 | 9.65 | 167.6813 | 145.17 | 4.68375 | 281.025 | 13.9875 | 22843.02 | 10016.89 | 87741 | 1386.25 | 995.5 | | 189 | 190. |
| | 10:20:00 | 28.38 | 9.54 | 168.345 | 144.045 | 4.08373 | 258.9 | 13.9875 | 23112.61 | 10016.89 | 88829 | 1384.875 | | | 189 | 190. |
| 7/20/2016 | | | | | | | | | 22760.08 | | | | | | 189 | |
| 7/20/2016 | 10:28:00 | 28.275 | 9.59 | 168.3 | 144.72 | 4.3125 | 258.75 | 13.9875 | | 9915.77 | 87516 | 1389.5 | | | | 190. |
| 7/20/2016 | 10:29:00 | 27.915 | 9.43 | 168.7725 | 142.92 | 4.3225 | 259.35 | 13.9875 | 23112.61 | | 87004 | 1389.75 | | 482.3 | 188.5 | 190. |
| 7/20/2016 | 10:30:00 | 28.185 | 9.64 | 168.7725 | 144.045 | 4.295 | 257.7 | 13.9875 | 22587.26 | 9921.388 | 86802 | 1394.625 | 995.8 | | 189 | 190. |
| 7/20/2016 | 10:31:00 | 28.56 | 9.735 | 168.1987 | 142.785 | 4.6875 | 281.25 | 13.9875 | 23188.65 | 10044.98 | 89272 | 1388.5 | | 482.3 | 188.5 | 190. |
| 7/20/2016 | 10:32:00 | 28.08 | 9.345 | 167.6362 | 143.325 | 4.69125 | 281.475 | 13.9875 | 22843.02 | 9938.242 | 88227 | 1385.75 | 993.7 | | 189 | 190. |
| 7/20/2016 | 10:33:00 | 28.62 | 9.405 | 169.245 | 142.695 | 4.31 | 258.6 | 13.9875 | 23382.2 | 10073.07 | 88584 | 1392.625 | | | 189 | 190. |
| 7/20/2016 | 10:34:00 | 28.635 | 9.66 | 168.1538 | 143.37 | 4.29375 | 257.625 | 13.9875 | 22836.11 | 9966.332 | 87221 | | 992.7 | 483.5 | 189.5 | 190. |
| 7/20/2016 | 10:35:00 | 28.59 | 9.635 | 167.7262 | 143.91 | 4.6875 | 281.25 | 13.9875 | 22932.89 | 9966.332 | 87975 | 1392.25 | 993.9 | 483.4 | 189.5 | |
| 7/20/2016 | | | 9.835 | | 145.08 | 4.31625 | 258.975 | 13.9875 | | | 87631 | 1395.5 | | | 189.5 | |
| 7/20/2016 | 10:37:00 | 28.425 | 9.58 | 168.3 | 143.955 | 4.31625 | 258.975 | 13.9875 | 22932.89 | 9966.332 | 87664 | 1392 | 994.6 | 483.8 | 189 | 190. |
| 7/20/2016 | 10:38:00 | 28.17 | 9.825 | 168.8625 | 145.35 | 4.30375 | 258.225 | 13.9875 | 22490.49 | 9966.332 | 86337 | 1393.625 | 993.6 | 482.6 | 189 | 190. |
| 7/20/2016 | 10:39:00 | 28.515 | 9.675 | 168.1987 | 144.18 | 4.6925 | 281.55 | 13.9875 | 22932.89 | 10078.69 | 88298 | 1389 | 994.2 | 483.1 | 188.5 | 190. |
| 7/20/2016 | 10:40:00 | | 9.59 | 166.7813 | 144.9 | 4.30375 | 258.225 | | 22670.21 | 10078.69 | 86830 | 1389.375 | 992.2 | 483.4 | 189 | 190. |
| 7/20/2016 | 10:41:00 | | 9.28 | 169.0988 | 142.38 | 4.305 | 258.3 | 13.9875 | 23195.56 | 9971.95 | 88983 | 1381.125 | 994 | 483.1 | 189 | 190. |
| 7/20/2016 | 10:42:00 | | | 168.6263 | 143.01 | 4.67125 | 280.275 | | | | 87527 | | | | | |
| 7/20/2016 | 10:43:00 | | | | 142.155 | 4.69 | 281.4 | | | | 89214 | 1378.5 | | | | |
| 7/20/2016 | 10:44:00 | | | | 143.37 | 4.29375 | 257.625 | 13.9875 | | | 87584 | | | | | |
| 7/20/2016 | 10:45:00 | | | | | 4.3075 | 258.45 | | | | 87319 | 1376.5 | | | | |
| 7/20/2016 | 10:45:00 | | | | 143.91 | 4.31125 | 258.675 | | 22939.8 | | 86957 | | | | | |
| 7/20/2016 | 10:47:00 | | | | 143.91 | 4.3125 | 258.75 | | | | 89766 | | | | | |
| 7/20/2016 | 10:47:00 | | | | | 4.3123 | 258.45 | | | | | 1377.625 | | | | |
| 7/20/2016 | 10:48:00 | | | | 143.125 | 4.3075 | 258.225 | | | | 88495 | | | | | |
| 7/20/2016 | | | | | | | | | | | | | | | | |
| | | | | | 145.665 | 4.3525 | 261.15 | | | | 87700 | | | | | |
| 7/20/2016 | 10:51:00 | 28.17 | 9.885 | 169.5263 | 144.585 | 4.2925 | 257.55 | 13.9875 | 22760.08 | 9943.86 | 88444 | 1374.5 | 994.6 | 483.8 | 189.5 | 191 |
| | A | | | 100.00 | 4 | | | | | 10040.00 | 00700.07 | 4704 05 | 003.03 | 400.00 | 100.00 | 400- |
| | Average | 28.34 | 9.63 | 168.42 | 152.59 | 4.41 | 264.52 | 14.09 | 22910.90 | 10010.26 | 88762.95 | 1381.98 | 993.82 | 483.28 | 188.80 | 189.7 |
| hik 20 2010 | | Manto FI- | | | | | · . | | Air Eleure | | | Tomneret | Urae | active the transmission | | |
| July 20, 2016 | | Waste Flo | | | A 11 11 | TOUC | TOUCH | Useel | Air Flows | Casarda | Charle | Temperat | /************************************* | Louise -t- | ICares Dr. | Charl |
| and the state of the | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | | Primary | Secondary | | SprayDryer | |
| | | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | PV-236 | PV-209c | FT-260c | TE-240 | TE-241 | TE-203 | TE-204 | TE-258 |
| Test1 | | 28.7 | 10.0 | 169.6 | 163.8 | 4.7 | 282.0 | 14.5 | J | 10179.8 | 95203.0 | L | 996.7 | 485.9 | 190.0 | |
| Max | WAXADOWNOL TANZ~~ | * | | | | | | | | | | | | | | 1 400 |
| | **** | 27.9 | | 166.4 | 142.2 | 4.3 | 256.7 | 13.4 | 22490.5 | 9904.5 | 86337.0 | 1366.3 | 989.3 | 480.6 | 187.5 | 189. |
| Max | | * | | | 142.2 152.6 | 4.3 | 256.7 264.5 | | 22490.5 22910.9 | | 86337.0 88763.0 | 1366.3 1382.0 | | | | |
| Max Min | 8783483555464755576557657657 CARGOLOGIACONCOLOGIA BERGERENSION | 27.9 | 9.3 | <u> </u> | 152.6 | | | 14.1 | 22910.9 | 10010.3 | | 1382.0 | 993.8 | 483.3 | 188.8 | 189 |

| TEST 1 | | Incinerator | | | BH dP | | HCI | CO2 | H2O | тнс | 02 | Opacity | | PAC |
|----------------|---|-------------|---|----------------------|----------|-------------------------------------|--|--------------------------------------|--|-----------------------------|--------------------------|---|--|--------------------|
| | | mmH2O | mmH2O | mmH2O | mmH2O | PPM | PPM | % | % | PPM | % | % | PPM | Lbs/h |
| Date | Time | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205COR | AT-213A | AT-213B | AT-213C | AT-259COR | AT-261 | AT-263 | AT-264 | SC-PAC-FT |
| 7/20/2016 | 9:51:00 | -0.7 | -22.8 | -53.2875 | 364.625 | 21.7 | 84.16 | 7.86 | 40.06 | 11.5 | 9 | 1.26 | 826.3 | 22.977 |
| 7/20/2016 | 9:52:00 | -9 | -31.75 | -65.55 | 335.125 | 21.6 | 84.13 | 7.88 | 40.06 | 10.9 | 8.91 | 1.3 | 833.8 | 22.262 |
| 7/20/2016 | 9:53:00 | -5.65 | -29.05 | -60.1875 | 347 | 20.8 | 82.56 | 7.82 | 40.06 | 11.5 | 8.94 | 1.3 | 829.6 | 22.213 |
| 7/20/2016 | 9:54:00 | -7.3 | -31.8 | -64.2375 | 336.0625 | 21 | 82.92 | 7.82 | 40.06 | 11.1 | 9.03 | 1.42 | 828.1 | 22.441 |
| 7/20/2016 | 9:55:00 | -6 | -30.2 | -60.7125 | 348.1875 | 21.3 | 83.44 | 7.79 | 40.06 | 11.9 | 9.11 | 1.48 | 815.2 | 22.961 |
| 7/20/2016 | 9:56:00 | -6.55 | -30.25 | -61.275 | 327.4375 | 20.6 | 84.01 | 7.8 | | 11 | 9.09 | 1.38 | 817.7 | 22.84 |
| 7/20/2016 | 9:57:00 | -5.55 | -30.4 | -57.6375 | 338.75 | 20.8 | 82.51 | 7.7 | | | 9.14 | 1.48 | 808.2 | 22.311 |
| 7/20/2016 | 9:58:00 | -5.55 | -29.35 | -57.2625 | 356.6875 | 22.2 | 83.72 | | | | 9.07 | 1.16 | 822.6 | 22.993 |
| 7/20/2016 | 9:59:00 | -2.95 | -26.7 | -52.3125 | 365.9375 | 22.1 | 84.07 | 7.91 | | | 8.93 | 1.26 | 832 | 22.246 |
| 7/20/2016 | 10:00:00 | -10.05 | -32.4 | -63.9375 | 336.0625 | 22.5 | 82.5 | | | | 8.84 | 1.28 | 844.5 | 22.766 |
| 7/20/2016 | 10:01:00 | -7,5 | -29.55 | -64.8 | 319.375 | 22.2 | 81.54 | | | | 8.85 | | 839.9 | 22.700 |
| 7/20/2016 | 10:02:00 | -8.65 | -31.7 | -62.775 | 341.375 | 21.1 | 80.93 | | | | 8.98 | | 827.1 | 22.896 |
| 7/20/2016 | 10:02:00 | -8.05 | -28 | -73.5375 | 288.4375 | 21.1 | 80.93 | | | | 9.01 | | 818.5 | 22.896 |
| 7/20/2016 | 10:03:00 | | -28 -29.8 | | | 21.2 | | 7.83 | | | 8.91 | | | |
| | | -6.6 | | -59.625 | 332.9375 | | 83.25 | | | | | | 821.2 | 22.766 |
| 7/20/2016 | 10:05:00 | -20.3 | -52.55 | -85.8 | 271 | 20.5 | 82.15 | 7.8 | | | 9 | | 818.2 | 22.928 |
| 7/20/2016 | 10:06:00 | -5.6 | -26.6 | -55.95 | 360.5625 | 20.2 | 82.15 | | | | 9.08 | | 824.2 | 22.39 |
| 7/20/2016 | 10:07:00 | -25.05 | -52.75 | -88.3875 | 261.5 | 19.9 | 83.58 | | | | 8.85 | | 838.4 | 22.863 |
| 7/20/2016 | 10:08:00 | -10.2 | -33.3 | -64.125 | 338.0625 | 20.4 | 83.57 | | | | 8.81 | | 843.9 | 23.026 |
| 7/20/2016 | 10:09:00 | -30.35 | -55.9 | -91.2 | 261.6875 | 20.7 | 82.77 | | | | 8.92 | | | 22.766 |
| 7/20/2016 | 10:10:00 | -9.25 | -31.4 | -63.75 | 337.875 | 20 | 82.82 | 7.83 | 40.06 | | 9.07 | 1.42 | 820.1 | 22.4 |
| 7/20/2016 | 10:11:00 | -27.1 | -53.15 | -89.4 | 260.9375 | 20.5 | 83.42 | 7.78 | 40.06 | 11.3 | 9.1 | 1.46 | 814.3 | 22.993 |
| 7/20/2016 | 10:12:00 | -7.8 | -30.6 | -60.9 | 328.875 | 21.4 | 84.32 | 7.75 | 40.06 | 11 | 9.16 | 1.41 | 808.8 | 22.9 |
| 7/20/2016 | 10:13:00 | -28.8 | -57.3 | -92.7375 | 267.125 | 20.7 | 83.49 | 7.72 | 40.06 | 12 | 9.23 | 1.45 | 806.7 | 22.993 |
| 7/20/2016 | 10:14:00 | -4.2 | -24.5 | -55.725 | 357.6875 | 22.4 | 83.41 | | | | 9.14 | | | 22.78 |
| 7/20/2016 | 10:15:00 | -31.4 | -59.3 | -94.8375 | 258.5625 | 22.7 | 83.82 | | | | 9.01 | | | 22.57 |
| 7/20/2016 | 10:16:00 | -9.6 | -33.05 | -64.5375 | 337.625 | 22.6 | 82.58 | | | | 8.97 | | | 22.40 |
| 7/20/2016 | 10:17:00 | -29.9 | -55.5 | -91.3125 | 263.8125 | 22.5 | 81.35 | | | | 9.01 | | | 22 |
| 7/20/2016 | 10:18:00 | -9.05 | -31.6 | -62.85 | 338.3125 | 22.5 | 81.63 | | | | 9.02 | | | 22.2 |
| 7/20/2016 | 10:19:00 | -24.6 | -46.6 | -86.175 | 286.9375 | 22.7 | 82.65 | | | | 9.06 | | | 22.24 |
| 7/20/2016 | 10:19:00 | -24.0 | -40.0 | -60.15 | 331.375 | 22.5 | | | | | 9.1 | | | 22.21 |
| | | | | | | | | | | | | | | |
| 7/20/2016 | 10:21:00 | -12.4 | -35.45 | -69 | 335.5 | 22.5 | | | | | | | | 22.278 |
| 7/20/2016 | 10:22:00 | -3.95 | -23.7 | -55.3125 | 358.9375 | 22.2 | | | | | 8.98 | | | 22.1 |
| 7/20/2016 | 10:23:00 | -16.75 | -41.55 | -76.0125 | 316.875 | 22.2 | | | | | | | | 22. |
| 7/20/2016 | 10:24:00 | -9.2 | -33.65 | -61.2375 | 341.625 | 24.1 | | 7.95 | 40.06 | 11 | 8.85 | | 844.9 | 22.24 |
| 7/20/2016 | 10:25:00 | -27.2 | -53.25 | -90.2625 | 282.9375 | 22.2 | 79.17 | 7,87 | 40.06 | 11.7 | 8.95 | 1.42 | 839.5 | 22.50 |
| 7/20/2016 | 10:26:00 | -7.35 | -30.6 | -60.9375 | 342.6875 | 22.8 | 79.09 | 7.87 | 40.06 | 11.2 | 8.98 | 1.41 | 827.2 | 22.37 |
| 7/20/2016 | 10:27:00 | -11.7 | -36.95 | -69.0375 | 316.375 | 22.8 | 81.23 | 7.87 | 40.06 | 11.4 | 8.99 | 1.38 | 821.5 | 22.89 |
| 7/20/2016 | 10:28:00 | -6.35 | -28.8 | -58.65 | 333.25 | 21.4 | 80.66 | 7.79 | 40.06 | 11.3 | 9.05 | 1.42 | 817.9 | 22. |
| 7/20/2016 | 10:29:00 | -8.3 | -31.7 | -63.6 | 349.75 | 22.8 | 78.94 | 7.73 | 40.06 | 11.9 | 9.12 | 1.32 | 817.9 | 22.9 |
| 7/20/2016 | 10:30:00 | -2.55 | -23.85 | -53.6625 | 361.75 | 24.4 | 80.16 | 7.91 | 40.06 | 11.5 | 8.99 | 1.16 | 828.9 | 22.76 |
| 7/20/2016 | | -14.75 | -39.25 | -68.775 | 325.1875 | 24.3 | | | | | 8.87 | | | 22 |
| 7/20/2016 | | -8.65 | -33.05 | -61.5375 | 341.375 | 24.9 | | | | | | | | 22.96 |
| 7/20/2016 | 10:33:00 | -11.6 | -36.35 | -68.2125 | | 23.4 | | | | | | | | 22 |
| 7/20/2016 | 10:33:00 | -6.85 | -30.9 | -60.375 | | 22.1 | | | | | | | | 22. |
| 7/20/2016 | | -0.83 | -32.35 | | 325.125 | 23.9 | | | | | | | | 22.76 |
| | | | | | | | | | | | | | | |
| 7/20/2016 | | -4.25 | -26.9 | | 338.3125 | 24.5 | | | | | | | | 22.1 |
| 7/20/2016 | | -6.6 | -28.95 | | | 24.4 | | | | | | | | 22 |
| 7/20/2016 | | -1.3 | -24.1 | | 362.0625 | 23.4 | | | | | | | | 22.96 |
| 7/20/2016 | | -13.35 | -37.45 | | 328.25 | 24 | | | | | | | | 22. |
| 7/20/2016 | | -6.9 | -30.5 | | 342.5625 | 24.4 | | | | | | | | 22 |
| 7/20/2016 | | -12.25 | -35.75 | | 330.75 | 22 | | | | | | | | |
| 7/20/2016 | 10:42:00 | -7.05 | -30.55 | -56.3625 | 343.5625 | 21.2 | 76.67 | 7.85 | 40.06 | 11.4 | 8.99 | 1.45 | 830 | 22.47 |
| 7/20/2016 | 10:43:00 | -10.65 | -37 | -64.575 | 320.8125 | 21.1 | 79.56 | 5 7.83 | 40.06 | 5 11.3 | 9.02 | 1.36 | 826.5 | 22.9 |
| 7/20/2016 | 10:44:00 | -3.75 | -27.8 | -56.925 | 335.125 | 20.3 | 78.71 | . 7.73 | 40.06 | 11.5 | 9.17 | 1.42 | 816.3 | 22. |
| 7/20/2016 | | -7.4 | -30.25 | | 349.625 | 20.9 | | . 7.71 | | | | | | |
| 7/20/2016 | | -2.65 | -24.7 | | 364.5 | 21.3 | | | | | | | | |
| 7/20/2016 | | -10.45 | -36.1 | | 328.9375 | 21.6 | | | | | | | | 2 |
| 7/20/2016 | | -7.35 | -29.45 | | | 22.9 | | | | | | | | |
| 7/20/2016 | | -7.55 | -25.45 | | 331.6875 | 21.3 | | | | | | | | |
| 7/20/2016 | | -9.4 | | | 344.5 | | | | | | | | | |
| | | | | | | | | | | | | | | |
| 7/20/2016 | 10:51:00 | -7 | -31.05 | -01.3125 | 324.4375 | 21.6 | 83.03 | 3 7.78 | 3 40.06 | 5 11.1 | 8.91 | 1.41 | 830 | 22.40 |
| | Average | -10.49 | -34.30 | -65.61 | 328.74 | 22.04 | 81.37 | 7.86 | 6 40.06 | 5 11.44 | 8.99 |) 1.36 | 828.15 | 23 |
| July 20, 2016 | | Pressures | Antonion An Incl. Minute Christ | SALAS VIEW DEVERSION | | Analyzers | | ang canadian a change and | Manufacture and the second second | un and a substant | no panalan panangang kan | 0140950012020000000000000000000000000000000 | | Flows |
| | | Incinerator | fanonana ana amin'ny fanonana amin'ny fanonana amin'ny fanonana amin'ny fanonana amin'ny fanonana amin'ny fanon | SD Outlet | Baghouse | со | НСІ | CO2 | H2O | ТНС | 02 | Opacity | SO2 | PACFlow |
| Test1 | and the second secon | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC- |
| Max | 7000704047070042010024004040 | -0.7 | -22.8 | | 365.9 | <i>ฉุ้านของสถานสามมากเหม</i> ากและเ | nfourieren en e | 000439425292539545689999999999999999 | and the second state of th | อสุ่งบรถเวลสองเสราะระจะเสรา | | telifertilmitti telessetentententetetetete | a sector de la companya de la compa | CONTRACTOR DISTORT |
| | | | -22.0 | | 258.6 | | | | | | ÷ | | -{ | |
| Min Average | C03420474004488040444 | -31.4 | | | | | 1 | | | | | | | |
| | | -10.5 | -34.3 | -65.6 | 328.7 | 22.0 | 81.4 | 7.9 | 9 40.1 | 11.4 | 9.0 |) 1.4 | 828.1 | |
| Variance | | 59.7832 | 83.95979 | 132.5637 | 841.0453 | 1.632459 | 4.173335 | 0.006201 | 1.85E-27 | 0.113792 | 0.012825 | 0.009112 | 130.1442 | 0.08 |

| EST 2 | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SDA | Stack |
|------------------------|---|----------------|--|--------------------------|------------------|----------------------------|--|--------------------|---------------------|--|----------------|---------------------|------------------|----------------|--------------|------------|
| | | LPM | LPM | LPM | LPM | LPM | SCFM | LPM | m3/h | annumproproproprogrammer and | | Degrees C | Degrees C | Degrees C | Degrees C | Degrees |
| | and the second se | | | FORMAL MARKEN CONTRACTOR | | | the second s | Lawrencemannessent | **** | here and the second sec | | encommencement | | | | TE-258 |
| 7/20/2016 | 11:06:00 | 28.23 | 9.73 | 168.0525 | 143.685 | 4.29375 | 257.625 | 13.9875 | 23029.66 | 9870.826 | 92344 | 1373 | 996.7 | 488.2 | 190 | 191 |
| 7/20/2016 | 11:07:00 | 28.26 | 9.595 | 169.29 | 144.225 | 4.2925 | 257.55 | 13.9875 | 22677.13 | 9971.95 | 86510 | 1369.625 | 997.2 | 489.9 | 190.5 | 191 |
| 7/20/2016 7/20/2016 | 11:08:00 11:09:00 | 28.17 28.56 | 9.435 9.575 | 167.9625 167.535 | 144.18 144.09 | 4.305 4.295 | 258.3 257.7 | 13.9875 13.9875 | 22856.85 22497.4 | 9859.59 9870.826 | 92597 87438 | 1374.125 1372.75 | 998 998.6 | 488.9 490.1 | 190.5 191 | 191 |
| 7/20/2016 | 11:10:00 | 28.095 | 10.015 | | 144.045 | 4.295 | 257.925 | 13.9875 | 22849.94 | 9870.826 | 93176 | 1372.75 | 998.3 | 490.1 | 191 | 191 191 |
| 7/20/2016 | 11:11:00 | 28.055 | 10.015 | 168.5812 | 145.305 | 4.23875 | 258.675 | 13.9875 | 22849.94 | 9994.422 | 88136 | 1371.375 | 996.9 | 488.6 | 190.5 | 191 |
| 7/20/2016 | 11:12:00 | 28.155 | 9.645 | 168.3 | 144.045 | 4.51125 | 271.575 | 13.9875 | 23119.52 | 9971.95 | 93037 | 1374.375 | 999.8 | 487.3 | 190.5 | 191 |
| 7/20/2016 | 11:13:00 | 28.5 | 9.84 | | 144.63 | 4.295 | 257.7 | 13.9875 | 22670.21 | | 87139 | 1369.75 | 1000.5 | 488.4 | 191 | 191 |
| 7/20/2016 | 11:14:00 | 28.41 | 9.65 | 168.0525 | 144.63 | 4.675 | 280.5 | 13.9875 | 23112.61 | | 93481 | 1373.5 | 999.2 | 487.3 | 190.5 | 192 |
| 7/20/2016 | 11:15:00 | 28.2 | 10.075 | 169.1437 | 145.125 | 4.31 | 258.6 | | 22677.13 | 9865.208 | 87720 | 1371.125 | 1000.4 | 487.9 | 191 | 191 |
| 7/20/2016 | 11:16:00 | 28.575 | 9.665 | 167.6362 | 144.225 | 4.69125 | 281.475 | 13.9875 | 23112.61 | | 92848 | 1371.875 | 999.5 | 487.4 | 190.5 | 190 |
| 7/20/2016 | 11:17:00 | 28.245 | 9.54 | 168.1987 | 144.09 | 4.68375 | 281.025 | 13.9875 | 22234.72 | 9887.68 | 86328 | 1373.875 | 999.6 | 487.9 | 190.5 | 190 |
| 7/20/2016 | 11:18:00 | 28.53 | 9.485 | | 144.09 | 4.67625 | 280.575 | 13.9875 | 23292.34 | 9988.804 | 92824 | 1376.125 | 999.6 | 487.4 | 190.5 | 1.90 |
| 7/20/2016 | 11:19:00 | 28.35 | 9.79 | 167.3438 | 144.585 | 4.67 | 280.2 | | 22766.99 | 9882.062 | 88429 | 1372.375 | 1001.6 | 489.6 | 191 | 191 |
| 7/20/2016 | 11:20:00 | 28.2 | 9.53 | 167.6362 | 143.865 | 4.6725 | 280.35 | 13.9875 | 23382.2 | 10000.04 | 92925 | 1370.375 | 1000.9 | 490.3 | 191.5 | 19: |
| 7/20/2016 | 11:21:00 | 28.44 | 9.845 | 169.4812 | 144.495 | 4.68125 | 280.875 | 13.9875 | 22856.85 | 9887.68 | 87773 | 1366.75 | 1002.9 | 491.7 | 192 | 19: |
| 7/20/2016 | 11:22:00 | 28.29 | 9.53 | 167.58 | 143.28 | 4.69375 | 281.625 | 13.9875 | 23112.61 | 9887.68 | 88856 | 1367.625 | 999.8 | 491.7 | 192 | 1 |
| 7/20/2016 | 11:23:00 | 28.44 | 9.81 | 169.29 | 145.35 | 4.68875 | 281.325 | 13.9875 | 22587.26 | 9769.702 | 86848 | 1371.25 | 1000.3 | 492.5 | 192.5 | 19: |
| 7/20/2016 | 11:24:00 | 28.2 | 9.81 | 168.9075 | 144.135 | 4.2925 | 257.55 | 13.9875 | 22939.8 | 9994.422 | 86742 | 1371.375 | 1002.4 | 491.1 | 192 | 19 |
| 7/20/2016 | 11:25:00 | 28.515 | 9.75 | 170.7075 | 145.8 | 4.6675 | 280.05 | 13.9875 | 22497.4 | 9859.59 | 86754 | 1374.125 | 1002.4 | 491.4 | 192 | 19 |
| 7/20/2016 | 11:26:00 | 28.02 | 9.67 | 166.5 | 144.495 | 4.3075 | 258.45 | 13.9875 | 23112.61 | 9859.59 | 88003 | 1375.125 | 1001.5 | 489 | 191.5 | 19 |
| 7/20/2016 | 11:27:00 | 28.335 | 9.745 | 168.0525 | 145.89 | 4.29625 | 257.775 | | 22587.26 | 9741.612 | 86511 | 1373.875 | 1002.4 | 488.2 | 191.5 | 19 |
| 7/20/2016 | 11:28:00 | 28.155 | 9.89 | 167.8163 | 144.675 | 4.69125 | 281.475 | | 22849.94 | 9943.86 | 88603 | 1372.625 | 1000.8 | 487.8 | 191 | 19 |
| 7/20/2016 | 11:29:00 | 28.245 | 9.855 | 169.9088 | 144.675 | 4.3175 | 259.05 | | 22677.13 | 9943.86 | 86907 | 1373 | 1002.8 | 488 | 191 | 19 |
| 7/20/2016 | 11:30:00 | 28.455 | 9.435 | | 144.045 | 4.69375 | 281.625 | | 23112.61 | | 87965 | 1376.375 | 1002.3 | 487.8 | 191 | 19 |
| 7/20/2016 | 11:31:00 | 27.945 | 9.855 | 167.9175 | 144.585 | 4.3125 | 258.75 | | 22587.26 | | 86838 | 1382.125 | 1004.3 | 488 | 191 | 19 |
| 7/20/2016 | 11:32:00 | 28.155 | 9.705 | | 143.415 | 4.69 | 281.4 | 13.9875 | 22856.85 | | 87429 | 1380.375 | 1002.5 | 487.9 | 191 | 19 |
| 7/20/2016 | 11:33:00 | 27.9 | 9.78 | 167.445 | 144.045 | 4.66125 | 279.675 | | 22497.4 | | 86151 | 1384.5 | 1003.8 | 486.9 | 191 | 19 |
| 7/20/2016 | 11:34:00 | 28.38 | 9.575 | | 143.415 | 4.67375 | 280.425 | | 23112.61 | | 88432 | | 1002.8 | 486.9 | 190.5 | |
| 7/20/2016 | 11:35:00 | 28.41 | 9.78 | 168.7725 | 145.89 | 4.67125 | 280.275 | | 22677.13 | | 87843 | 1381.5 | 1001.3 | 487.6 | 191 | 19 |
| 7/20/2016 | 11:36:00 | 28.215 | 9.915 | 167.58 | 144.45 | 4.69 | 281.4 | | 22939.8 | | 88193 | 1382.25 | 1002.7 | 488.3 | 191 | |
| 7/20/2016 | 11:37:00 | 28.635 | 9.985 | | 146.16 | 4.3175 | 259.05 | | 22766.99 | | 86630 | 1384.75 | 1001.7 | 487.9 | 191 | |
| 7/20/2016 | 11:38:00 | 28.095 | 9.825 | | 144.765 | 4.7 | 282 | | 22849.94 | | 87556 | | 999 | 487.9 | 191 | |
| 7/20/2016 | 11:39:00 | 28.305 | 10.195 | 168.2438 | 146.025 | 4.3175 | 280.8 | | 22497.4 | | 85688 | 1386 | 1002.8 | 487.7 | 191 | 19 |
| 7/20/2016 | 11:40:00 | 28.02 | 9.505 | 169.335 | 144.9 | 4.31375 | 258.825 | | 22677.13 | | 87202 | | 1002.6 | 487.8 | 190.5 | |
| 7/20/2016 | 11:41:00 | 28.14 | 9.745 | | 144.9 | 4.30625 | 258.375 | | 22324.59 | | 85899 | 1388.625 | 1002.2 | 487 | 190.5 | |
| 7/20/2016 7/20/2016 | 11:42:00 11:43:00 | 28.05 28.32 | 9.53 9.555 | 167.8725 168.3 | 143.46 144.63 | 4.31375 4.29625 | 258.825 257.775 | | 22939.8 22760.08 | | 88107 87000 | 1381.875 1381.25 | 1000.5 1003.6 | 488.4 489.2 | 190 191 | |
| 7/20/2016 | 11:43:00 | 28.32 | 9.39 | 167.9625 | 144.03 | 4.29623 | 280.35 | | 22939.8 | | 88088 | | 1003.8 | 489.2 | 191 | |
| 7/20/2016 | 11:45:00 | 28.335 | 9.6 | 168.6712 | 144.045 | 4.66625 | 279.975 | | 22587.26 | | 86726 | 1373.375 | | 486.1 | 191.5 | |
| 7/20/2016 | 11:46:00 | 28.335 | 9.625 | 168.48 | 143.46 | 4.67375 | 280.425 | | 22587.26 | | 88321 | 1378.75 | 1003.1 | 485.5 | 191.5 | |
| 7/20/2016 | 11:47:00 | 28.29 | 9.79 | 169.8525 | 146.16 | 4.315 | 258.9 | | 22407.54 | | 86194 | 1380.75 | 1001.6 | 485 | 191 | |
| 7/20/2016 | 11:48:00 | 28.29 | 9.935 | 168.8175 | 145.395 | 4.315 | 258.9 | | 22587.26 | | 87494 | 1378 | 1002.3 | 485.8 | 190.5 | |
| 7/20/2016 | 11:49:00 | 28.38 | 9.95 | | 146.025 | 4.68625 | 281.175 | | 22497.4 | | 86473 | | 1003.2 | | 190 | |
| 7/20/2016 | 11:50:00 | 28.32 | 10.025 | | 145.575 | 4.315 | 258.9 | | 22849.94 | | 87900 | 1377.5 | | 486.2 | 190 | |
| | | 28.29 | 10.03 | | 146.115 | 4.67 | 280.2 | | 22677.13 | | 88270 | 1380.25 | | | 190 | |
| 7/20/2016 | 11:52:00 | 28.17 | 9.495 | | 144.945 | | 279.525 | | 22760.08 | | 88340 | | | | 190 | |
| 7/20/2016 | 11:53:00 | 28.275 | 9.76 | 166.545 | 144.945 | | 280.575 | | 22760.08 | | 87007 | 1374.5 | | | 190 | |
| 7/20/2016 | 11:54:00 | 28.44 | 9.35 | 168.39 | 143.28 | | 280.275 | | 22587.26 | | 87648 | 1371.75 | | | 190 | |
| 7/20/2016 | 11:55:00 | 28.38 | 9.49 | | 145.26 | | 280.725 | | 22760.08 | | 86828 | 1376.25 | | | 190.5 | |
| 7/20/2016 | 11:56:00 | 28.2 | 9.565 | 169.2 | | 4.67125 | 280.275 | | 22766.99 | | 86281 | | | | 190.5 | |
| 7/20/2016 | 11:57:00 | 28.05 | | 167.9625 | 144.765 | 4.67875 | 280.725 | | 22407.54 | | 85356 | | | | 190 | |
| 7/20/2016 | 11:58:00 | 28.29 | | 170.4713 | 144.225 | | 281.475 | | 22856.85 | | 87737 | 1376 | | | 190.5 | |
| 7/20/2016 | 11:59:00 | 27.99 | 9.69 | 166.9725 | 146.07 | 4.69375 | 281.625 | 13.9875 | 22677.13 | 9780.938 | 86485 | 1377.625 | 1001.8 | 488 | 190.5 | |
| 7/20/2016 | 12:00:00 | 28.29 | 9.77 | 170.1 | 145.98 | 4.3175 | 259.05 | 13.9875 | 22677.13 | 9775.32 | 88216 | 1372 | 1002.5 | 488.1 | 190.5 | 19 |
| 7/20/2016 | 12:01:00 | 28.53 | 9.55 | 167.2987 | 146.61 | 4.3125 | 258.75 | 13.9875 | 22497.4 | 9876.444 | 89631 | 1378.125 | 1001.4 | 486.8 | 190.5 | 19 |
| 7/20/2016 | 12:02:00 | 27.945 | 9.92 | 169.0988 | 145.98 | 4.67125 | 280.275 | 13.9875 | 22580.35 | 9876.444 | 87136 | 1375.375 | 1001.1 | 488.1 | 190.5 | 19 |
| 7/20/2016 | 12:03:00 | 28.275 | 9.765 | 166.635 | 145.89 | 4.67 | 280.2 | 13.9875 | 22587.26 | 9764.084 | 93199 | 1382.375 | 1002.4 | 487.3 | 190 | 19 |
| 7/20/2016 | 12:04:00 | 28.125 | 9.835 | 168.6263 | 145.53 | 4.67625 | 280.575 | 13.9875 | 22504.31 | 9780.938 | 86019 | 1381.75 | 1003.3 | 487.8 | 190 | 19 |
| 7/20/2016 | 12:05:00 | 28.035 | 9.45 | 169.0988 | 144.405 | 4.6625 | 279.75 | 13.9875 | 22684.04 | 9775.32 | 92973 | 1385.875 | 1002.3 | 485 | 189.5 | 1 |
| 7/20/2016 | 12:06:00 | 28.155 | 9.815 | 167.4 | 144.36 | 4.67625 | 280.575 | 13.9875 | 22760.08 | 9668.578 | 87739 | 1376.875 | 1003.5 | 487.6 | 189.5 | 1 |
| | Average | 28.27 | 9.72 | 168.35 | 144.75 | 4.53 | 272.14 | 13.99 | 22753.28 | 9853.97 | 88244.64 | 1376.86 | 1001.33 | 488.02 | 190.74 | 19 |
| uly 20, 2016 | | Waste Flow | CONSCIENCES (CONSCIENCE) IN THE OWNER OF THE OWNER | | P | Contraction and the factor | | | Air Flows | | | Temperatu | | | | |
| | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SprayDryer | Stack |
| lest1 | | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | PV-236 | PV-209c | FT-260c | TE-240 | TE-241 | TE-203 | TE-204 | TE-258 |
| Max | | 28.6 | 10.2 | 170.7 | 146.6 | 4.7 | 282.0 | 14.0 | 23382.2 | 10000.0 | 93481.0 | 1388.6 | 1004.3 | 492.5 | 192.5 | 19 |
| Vin | | 27.9 | 9.4 | 166.5 | 143.3 | 4.3 | 257.6 | 14.0 | 22234.7 | 9668.6 | 85356.0 | 1366.8 | 996.7 | 484.3 | 189.5 | 19 |
| Average | | 28.3 | 9.7 | 168.4 | 144.7 | 4.5 | 272.1 | 14.0 | 22753.3 | 9854.0 | 88244.6 | 1376.9 | 1001.3 | 488.0 | 190.7 | 19 |
| | | | | | | | | | | | | | | | | |

| Date 7/20/2016 7/20/2016 7/20/2016 7/20/2016 7/20/2016 7/20/2016 7/20/2016 | | morner water over the second | mmH2O PT-249 | hanne and the second | mmH2O | PPM | PPM | % | % | PPM | % | % | PPM | Lbs/h |
|--|-------------|--|---|--|--|--------------------------|---|--|--|-----------|--|--|--|-----------|
| 7/20/2016 7/20/2016 7/20/2016 7/20/2016 7/20/2016 | 11:06:00 | mymemererererererererererererererererere | PT-249 | DT CIC | | | | | | | | CONSISTER OF A DESCRIPTION OF A DESCRIPT | | |
| 7/20/2016 7/20/2016 7/20/2016 7/20/2016 | | | 010000000000000000000000000000000000000 | Concernance of the local division of the loc | PDT-622 | AT-205COR | | AT-213B | AT-213C | AT-259COF | | AT-263 | CONTRACTOR CONTRACTOR | SC-PAC-F1 |
| 7/20/2016 7/20/2016 7/20/2016 | 11.() / (1) | -19.75 | -48.65 | -64.35 | 269.75 | 18.7 | 85.11 | | 40.06 | 11.4 | 8.84 | 1.48 | 847.6 | 22.408 |
| 7/20/2016 7/20/2016 | | -5.3 | -27.1 | -55.875 | 333.25 | 18.7 | 86.46 | | 40.06 | | 8.77 | 1.46 | 847.6 | 22.798 |
| 7/20/2016 | 11:08:00 | -26.15 | -52.4 | -65.6625 | 267 | 19.6 | 86.33 | | 40.06 | | 8.9 | 1.52 | 844.2 | 22.2 |
| | 11:09:00 | -4.85 | -26.25 | -48.675 | 359.75 | 19.3 | 87.06 | | 40.06 | | 8.97 | 1.2 | 850.4 | 22.863 |
| 7/20/2016 | 11:10:00 | -26.8 | -56.05 | -69.3 | 260 | 19.2 | 88.79 | | 40.06 | | 8.71 | 1.3 | 863.6 | 22.97 |
| | 11:11:00 | -7.45 | -31.25 | -64.0875 | 335.75 | 20.5 | 88.4 | | 40.06 | | 8.67 | 1.32 | 872 | 22.8 |
| 7/20/2016 | 11:12:00 | -26.3 | -52.5 | -80.1 | | 20.2 | 87.9 | | 40.06 | | 8.72 | 1.42 | 864.5 | 22.19 |
| 7/20/2016 | 11:13:00 | -7.65 | -31.45 | -60.975 | 337.5 | 19.2 | 88.6 | | 40.06 | | 8.85 | 1.5 | 855.9 | 22.2 |
| 7/20/2016 | 11:14:00 | -25.9 | -54.3 | -74.8875 | 262.625 | 19.1 | 89.71 | | 40.06 | | 8.86 | 1.5 | 854.6 | 23. |
| 7/20/2016 | 11:15:00 | -4.85 | -28.85 | -57.975 | 330.4375 | 18.9 | 89.73 | | 40.06 | | 8.83 | 1.48 | 848 | 22.45 |
| 7/20/2016 | 11:16:00 | -27.65 | -56.15 | -76.875 | 294.8125 | 18.5 | 89.46 | | 40.06 | | 8.96 | 1.48 | 845.7 | 22.538 |
| 7/20/2016 | 11:17:00 | -3.95 | -28.8 | -55.9875 | 356.6875 | 18.9 | 90.66 | | 40.06 | | 8.87 | 1.36 | 860.6 | 22.766 |
| 7/20/2016 | 11:18:00 | -30.65 | -59.45 | -76.6125 | 281.4375 | 19.3 | 91.27 | 8.08 | 40.06 | 11.6 | 8.72 | 1.42 | 870.3 | 22.26 |
| 7/20/2016 | 11:19:00 | -7.45 | -31.85 | -59.5875 | 337.0625 | 19 | 91.22 | 8.06 | 40.06 | 10.7 | 8.64 | 1.33 | 873.3 | 22.246 |
| 7/20/2016 | 11:20:00 | -28.75 | -58 | -71.2875 | 268.5625 | 17.7 | 90.41 | 7.97 | 40.06 | 11.2 | 8.75 | 1.45 | 866.3 | 22.473 |
| 7/20/2016 | 11:21:00 | -6.25 | -29.95 | -58.1625 | 339.375 | 18.5 | 91.93 | 7.9 | 40.06 | 10.8 | 8.87 | 1.46 | 846.5 | 22.993 |
| 7/20/2016 | 11:22:00 | -15.05 | -36.7 | -71.925 | 304.125 | 18.5 | 93.27 | 7.87 | 40.06 | 11 | 8.87 | 1.5 | 841.9 | 22. |
| 7/20/2016 | 11:23:00 | -3.7 | -26.75 | -46.9875 | 330.375 | 18 | 94.52 | 7.86 | 40.06 | 11 | 8.92 | 1.5 | 842.3 | 22.993 |
| 7/20/2016 | 11:24:00 | -7 | -31.4 | -64.725 | 340.5 | 18.4 | 94.04 | 7.86 | 40.06 | 11.2 | 8.95 | 1.42 | 844.4 | 22.343 |
| 7/20/2016 | 11:25:00 | -0.95 | -23.65 | -53.1 | 359.25 | 18.9 | 95.42 | 8.01 | 40.06 | 11.1 | 8.77 | 1.32 | 866.2 | 22.5 |
| 7/20/2016 | 11:26:00 | -12.75 | -38.75 | -73.875 | 324.375 | 18.9 | 95.42 | | 40.06 | | 8.68 | 1.46 | 871.8 | 22.213 |
| 7/20/2016 | 11:27:00 | -5.7 | -30.7 | -55.9875 | 339.75 | 19.9 | 94.49 | | 40.06 | | 8.55 | 1.33 | 883.3 | 23.026 |
| 7/20/2016 | 11:28:00 | -13.85 | -37.8 | -76.05 | 323.8125 | 19.4 | 93.72 | | 40.06 | | 8.7 | 1.46 | 875 | 22.97 |
| 7/20/2016 | 11:29:00 | -6 | -30.35 | -58.125 | 343.25 | 18.9 | 93.77 | | 40.06 | | 8.75 | 1.48 | 865.6 | 22.961 |
| 7/20/2016 | 11:30:00 | -9.4 | -34.75 | -66.4125 | 318.125 | 19.5 | 95.02 | | 40.06 | | 8.76 | | 862.3 | 22.5 |
| 7/20/2016 | 11:31:00 | -3.3 | -27.85 | -52.8375 | 334.5625 | 20.7 | 94.71 | | 40.06 | | 8.82 | | | |
| 7/20/2016 | 11:32:00 | -5.85 | -30.9 | -60.075 | 350 | 20.9 | 92.95 | | 40.06 | | 8.94 | 1.32 | | 22.52 |
| 7/20/2016 | 11:33:00 | -0.25 | -23.15 | -57.675 | 361.25 | 21 | 93.86 | | | | 8.76 | | | |
| 7/20/2016 | 11:34:00 | -9.3 | -33.55 | | 324.125 | 22.2 | 93.44 | | 40.06 | | 8.68 | | | 22.97 |
| 7/20/2016 | 11:35:00 | -5.2 | -30.25 | | 339.8125 | 22.1 | 91.44 | | 40.06 | | 8.55 | | | |
| 7/20/2016 | 11:35:00 | -9.15 | -34.6 | | 334.375 | 21.1 | 90.39 | | 40.06 | | 8.63 | | | |
| | | -2.75 | | | | | | | | | | | | |
| 7/20/2016 | 11:37:00 | | -25.15 | | 347.375 | 21.5 | 89.1 | | | | 8.74 | | | |
| 7/20/2016 | 11:38:00 | -6.9 | -31.15 | | 326.875 | 22.3 | 90.46 | | | | 8.71 | | | |
| 7/20/2016 | 11:39:00 | -2.4 | -25.2 | -48.075 | 338.5 | 22.4 | 90.71 | | | | 8.73 | | | |
| 7/20/2016 | 11:40:00 | -5.7 | -31.45 | | 354.1875 | 22.3 | 88.75 | | | | 8.83 | | | |
| 7/20/2016 | 11:41:00 | -0.65 | -24.1 | -47.1 | 363.4375 | 23.5 | 89.31 | | | | 8.6 | | | |
| 7/20/2016 | 11:42:00 | -11.35 | -37.45 | | 330.375 | 24.3 | 89.45 | | | | 8.53 | | | |
| 7/20/2016 | 11:43:00 | -4.8 | -29.35 | -49.35 | 344.5 | 23.3 | 87.84 | | | | 8.54 | | | |
| 7/20/2016 | 11:44:00 | -12.2 | -37.6 | | | 20.3 | 85.98 | | | | 8.75 | | | |
| 7/20/2016 | 11:45:00 | -5.1 | -28.75 | -58.575 | 342.75 | 20.2 | 88.16 | | | | 8.94 | | | |
| 7/20/2016 | 11:46:00 | -7.75 | -33.15 | | 320.6875 | 19.8 | 89.59 | | | | 8.93 | | | |
| 7/20/2016 | 11:47:00 | -3.4 | -27.4 | -53.7375 | 334.6875 | 20.3 | 88.65 | | | | 9 | | | |
| 7/20/2016 | 11:48:00 | -3.8 | -26.7 | -54.1125 | 350.5625 | 20.5 | 88.05 | 7.81 | 40.06 | 5 11.6 | 9.04 | 1.26 | | |
| 7/20/2016 | 11:49:00 | -2.15 | -24.55 | -45.1125 | 360.25 | 21.3 | 89.6 | 8 | 40.06 | 5 12.3 | 8.77 | 1.16 | 870.4 | 22.96 |
| 7/20/2016 | 11:50:00 | -8.55 | -31.55 | ~63.525 | 329.625 | 23.6 | 88.15 | 8.06 | 40.06 | 5 10.9 | 8.63 | 1.26 | 879.1 | 22.246 |
| 7/20/2016 | | -6.15 | -30.65 | -52.05 | 342.9375 | 23.2 | 86.8 | 8.05 | | | 8.64 | 1.33 | | |
| 7/20/2016 | 11:52:00 | -9.15 | -33.95 | -56.775 | 332.6875 | 20.7 | 86.48 | 3 7.95 | 40.06 | 5 11.2 | 8.81 | 1.38 | 866.3 | 22.27 |
| 7/20/2016 | 11:53:00 | -6.5 | -31.3 | -54.2625 | 344.625 | 20.7 | 86.86 | 5 7.91 | 40.06 | 5 11 | 8.86 | 1.46 | 856.3 | 22.79 |
| 7/20/2016 | 11:54:00 | -6.55 | -30.25 | -67.725 | 324.4375 | 19.2 | 88.29 | 7.88 | 40.06 | 5 10.6 | 8.82 | 1.42 | 849.6 | 22.5 |
| 7/20/2016 | 11:55:00 | -2.4 | -25.35 | -57.3375 | 337 | 18.8 | 88.82 | 7.84 | 40.06 | 5 11.1 | 8.93 | 1.48 | 843.5 | 22.3 |
| 7/20/2016 | 11:56:00 | -4.05 | -27.65 | | 352.875 | 20.1 | 89.58 | 7.86 | 40.06 | 5 11 | 9.04 | 1.16 | 852.7 | 22.4 |
| 7/20/2016 | | -0.3 | -20.95 | | | 21.5 | 90.5 | 8.03 | 40.06 | | | 1.21 | 872.3 | 22.6 |
| 7/20/2016 | 11:58:00 | -7.45 | -33.85 | | | 21.9 | 90.14 | 8.06 | | | | | | |
| 7/20/2016 | 11:59:00 | -4.7 | -30.1 | | | 21.7 | 88.2 | | | | | | | |
| 7/20/2016 | 12:00:00 | -6.75 | -29.9 | | 335.75 | | 88.33 | | | | | | | |
| 7/20/2016 | 12:01:00 | -10.55 | -41.25 | | 286.375 | | 89.85 | | | | | | | |
| 7/20/2016 | 12:02:00 | -5.05 | -28.5 | | 326.625 | | 89.79 | | | | | | | |
| 7/20/2016 | 12:03:00 | -21.55 | -51.1 | | 281.875 | | 88.68 | | | | | | | |
| 7/20/2016 | 12:04:00 | -2 | -25.45 | | 354.875 | | 89.31 | | | | | | | |
| | 12:05:00 | -24.65 | -54.5 | | | | 89.96 | | | | | | | |
| 7/20/2016 | | -24.05 | -31.9 | | 333.5 | | 89.19 | | | | | | | |
| | Average | -9.34 | • | | 326.84 | | 90.07 | | | | | | | |
| uly 20, 2016 | | Pressures | | | | Analyzers | | | | | | | | Flows |
| | | | SDA Inlet | SD Outlet | Baghouse | со | HCI | CO2 | H2O | THC | 02 | Opacity | SO2 | PACFlov |
| Test1 | | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC- |
| | | | CONTRACTOR OF | aparana a a a a a a a a a a a a a a a a a | (moderna and south and sou | สุดกระบบความสาวสาวสาวสาว | CONSTRUCTION OF THE OWNER | | a a second s | | Contraction of the local distances of the loc | | ะปู้งานของเหตุ (1996) | |
| Max | | -0.3 | -21.0 | + | 363.4 | | 95.4 | | | | | | | |
| Min | 4 | -30.7 | -59.5 | 1 | 260.0 | | 85.1 | | | | | | | |
| Average Variance | ***** | -9.3 65.13784 | -34.2 97.93811 | | 326.8 803.2456 | | 90.1 6.661485 | ~}~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | | | | | | |

| TEST 3 | | § | | | | | | | | Secondary | | | Secondary | | SDA | Stack |
|----------------|----------|---|---------------|---|-------------------|--------------------|-------------------|---|----------------------|-----------|----------------|----------------------|----------------------------|----------------|--|--|
| | | LPM | LPM | A CONTRACTOR OF | LPM | | SCFM | LPM | m3/h | m3/h | m3/h | | Degrees C | | Degrees C | NUMBER OF THE OWNER OWNER OF THE OWNER OWNE |
| | | and the second second second second | | STREET CAPETRICOM CONCERNMENT | PV-207 | CONTRACTOR DATA | | New Work William Strategy and Str | PV-236 | PV-209 | FT-260C | | hanannoverannaturever | TE-203 | A CONTRACTOR OF A CONTRACTOR O | TE-258 |
| 7/20/2016 | | 28.215 | 9.63 | 167.2538 | 143.73 | 4.3075 | 258.45 | 13.9875 | 23112.61 | 9904.534 | 89355 | 1376.375 | 1002.6 | 486.3 | 189.5 | 191.: |
| 7/20/2016 | | 28.08 | 9.585 | 166.635 | 144.315 | 4.6925 | 280.275 | 13.9875 | 22849.94 | 9786.556 | 87258 | 1377 | 1004.4 | 487.8 | 190 | 191.: |
| 7/20/2016 | | 28.125 | 9.625 | 170.19 | 144.315 | 4.30125 | 258.075 | 13.9875 | 23119.52 | | 91497 | 1375.375 | 1006.8 | 487.7 | 190 | 191. |
| 7/20/2016 | | 28.02 | 10.065 | 167.2538 | 145.485 | 4.68875 | 281.325 | 13.9875 | 22766.99 | 9691.05 | 86168 | 1373 | 1003.8 | 488.6 | | 191.: |
| 7/20/2016 | | 28.29 | 9.825 | 168.8175 | 144.9 | 4.68 | 280.8 | 13.9875 | 22849.94 | | 88317 | 1374.375 | 1005.1 | 488.4 | 190 | 192.4 |
| 7/20/2016 | | 28.14 28.335 | 9.935 9.77 | 168.0075 168.435 | 145.44 | 4.6725 | 280.35 279.975 | 13.9875 13.9875 | 22677.13 | | 86402 87534 | 1375.875 1377.375 | 1005.1 1004 | 489.2 489.5 | | 19: 19: |
| 5 1975 1994 19 | | 28.33 | 9.88 | 167.2987 | 144.765 145.89 | 4.66625 4.68625 | 279.975 | 13.9875 | 23119.52 22766.99 | | 85566 | 1377.375 | 1004 | 489.1 | 190.5 | 19. |
| 7/20/2016 | | 28.22 | 9.64 | 167.445 | 143.505 | 4.66875 | 280.125 | 13.9875 | 23036.58 | | 88285 | 1380.625 | 1006.2 | 489.3 | | 191 |
| 7/20/2016 | | 28.215 | 9.93 | 168.39 | 143.303 | 4.00873 | 257.55 | 13.9875 | 22677.13 | | 87450 | 1381.125 | 1000.2 | 485.5 | | 19: |
| 7/20/2016 | | 28.5 | 9.52 | | 144.045 | 4.2525 | 280.05 | 13.9875 | 23126.44 | | 89301 | 1377.625 | 1004.8 | 490 | | 192.3 |
| 7/20/2016 | | 28.155 | 9.76 | 167.1525 | 144.045 | 4.69875 | 281.925 | 13.9875 | 22766.99 | | 87094 | 1380 | 1005.4 | 490.6 | | 192.3 |
| 7/20/2016 | | | 9.69 | 168.0075 | 142.83 | 4.66875 | 280.125 | 13.9875 | 22677.13 | 9831.5 | 87283 | 1376.75 | 1004 | 490.6 | | 192.3 |
| 7/20/2016 | | | 9.56 | 168.435 | 139.995 | 4.67125 | 280.275 | 13.9875 | 22497.4 | | 85771 | | 1003.8 | 490.6 | | 192.1 |
| 7/20/2016 | | | 9.84 | 168.9525 | 139.275 | 4.6725 | 280.35 | 13.9875 | 22766.99 | 9831.5 | 87631 | 1378.5 | 1005.2 | 491 | | 192.1 |
| 7/20/2016 | | | 10.22 | 168.345 | 140.67 | 4.68125 | 280.875 | 13.9875 | 22414.45 | | 87244 | 1385.125 | 1005.5 | 490.1 | | 192.1 |
| 7/20/2016 | | | 9.985 | 168.5363 | 139.95 | 4.3075 | 258.45 | 13.9875 | 22856.85 | | 87884 | 1379.25 | 1007.6 | 489.4 | | 192.1 |
| 7/20/2016 | | | 9.975 | 169.5712 | 140.535 | 4.69 | 281.4 | 15.5675 | 22324.59 | | 87078 | 1378.125 | 1006.1 | 486.9 | | 192.1 |
| 7/20/2016 | | | 10.06 | 168.1087 | 139.635 | 4.6725 | 280.35 | 13.95 | 23119.52 | | 87894 | 1372.625 | 1003.3 | 485.5 | | 192.3 |
| 7/20/2016 | | | 9.925 | 168.435 | 140.85 | 4.295 | 257.7 | 14.2125 | 22766.99 | | 86532 | | 1005.1 | 483.5 | | 192.1 |
| 7/20/2016 | | | 9.92 | | 138.645 | 4.6675 | 280.05 | 14.2125 | 22946.71 | | 87449 | 1372.125 | 1004.3 | 482.5 | | 192.: |
| 7/20/2016 | | | 10.015 | 168.0075 | 138.645 | 4.68125 | 280.875 | 14.2125 | 22760.08 | | 86359 | 1376 | 1004.7 | 480.3 | | 192. |
| 7/20/2016 | | | 9.63 | 169.7175 | 138.105 | 4.30125 | 258.075 | 14.2125 | 22677.13 | | 87068 | 1371 | 1003.7 | 481.4 | | 191. |
| 7/20/2016 | | | 9.86 | 166.545 | 138.69 | 4.67 | 280.2 | 14.2125 | 22497.4 | | 85504 | 1374.125 | 1002.1 | | | 191. |
| 7/20/2016 | | | 9.745 | 168.0075 | 138.15 | 4.6775 | 280.65 | 14.2125 | 22939.8 | 9887.68 | 88724 | 1366.125 | 1002.1 | | | 190. |
| 7/20/2016 | | | 9.98 | 170.3812 | 139.23 | 4.67625 | 280.575 | 14.2125 | 22587.26 | | 85831 | 1367.375 | 1001.1 | 482.5 | 188.5 | 190. |
| 7/20/2016 | | | 9.805 | 167.49 | 139.23 | 4.66875 | 280.125 | 14.2125 | 22849.94 | | 88104 | 1359.5 | | | | 191. |
| 7/20/2016 | 12:48:00 | 27.36 | 10.175 | 168.0075 | 140.535 | 4.68375 | 281.025 | 14.2125 | 22684.04 | 9674.196 | 87143 | 1366.25 | 999.2 | 483.1 | . 189 | 191. |
| 7/20/2016 | 12:49:00 | 27.105 | 10 | 170.9437 | 139.545 | 4.685 | 281.1 | 14.2125 | 22587.26 | 9780.938 | 87637 | 1361.875 | 997.8 | 483.7 | 188.5 | 191. |
| 7/20/2016 | 12:50:00 | 27.33 | 9.93 | 168.6712 | 140.085 | 4.67875 | 280.725 | 14.2125 | 22587.26 | 9674.196 | 86488 | 1366 | 1001.2 | 481.9 | 188.5 | 190. |
| 7/20/2016 | 12:51:00 | 26.82 | 9.955 | 169.7625 | 139.455 | 4.68875 | 281.325 | 14.2125 | 22677.13 | 9831.5 | 87623 | 1365.5 | 998.1 | 482.2 | 188 | 190. |
| 7/20/2016 | 12:52:00 | 27.24 | 9.86 | 169.0087 | 140.535 | 4.66625 | 279.975 | 14.2125 | 22497.4 | 9730.376 | 85431 | 1373.375 | 998.2 | 481.3 | 187.5 | 190. |
| 7/20/2016 | 12:53:00 | 27.345 | 9.78 | 169.9088 | 138.105 | 4.6775 | 280.65 | 14.2125 | 22677.13 | 9719.14 | 89107 | 1368.375 | 996.7 | 476.2 | . 187 | 190. |
| 7/20/2016 | 12:54:00 | 27.27 | 9.885 | 167.1075 | 138.105 | 4.67875 | 280.725 | 14.2125 | 22677.13 | 9719.14 | 87160 | 1365.25 | 999.8 | 479.6 | 187 | 189.6 |
| 7/20/2016 | 12:55:00 | 27.39 | 9.65 | 168.5812 | 138.105 | 4.67875 | 280.725 | 14.2125 | 22856.85 | 9735.994 | 87591 | 1363.875 | 996.4 | 483.5 | 187.5 | 190. |
| 7/20/2016 | 12:56:00 | 27.12 | 9.67 | 170.5162 | 138.69 | 4.66875 | 280.125 | 14.2125 | 22497.4 | 9735.994 | 88059 | 1366.625 | 999.5 | 479.2 | 187.5 | 190. |
| 7/20/2016 | 12:57:00 | 27.375 | 9.9 | 170.145 | 138.69 | 4.67875 | 280.725 | 14.2125 | 22684.04 | 9735.994 | 87120 | 1362.875 | 997.5 | 473.8 | 187 | 190. |
| 7/20/2016 | 12:58:00 | 27.39 | 9.615 | 169.5263 | 138.6 | 4.69125 | 281.475 | 14.2125 | 22504.31 | 9618.016 | 87463 | 1369.625 | 997.3 | 468.3 | 185.5 | 189.0 |
| 7/20/2016 | 12:59:00 | 27.36 | 9.965 | 169.9088 | 139.725 | 4.69 | 281.4 | 14.2125 | 22497.4 | 9623.634 | 87611 | 1366.75 | 999.4 | 466.5 | 184.5 | 189. |
| 7/20/2016 | 13:00:00 | 27.6 | 10.08 | 168.435 | 139.635 | 4.3175 | 259.05 | 14.2125 | 22497.4 | 9623.634 | 91172 | 1372.375 | 998.7 | 464.1 | . 183.5 | 188. |
| 7/20/2016 | 13:01:00 | 27.375 | 9.945 | 169.7175 | 142.65 | 4.3175 | 259.05 | 14.2125 | 22677.13 | 9724.758 | 89330 | 1367.25 | 997.8 | 465.7 | 182.5 | 188. |
| 7/20/2016 | 13:02:00 | 27.435 | 9.945 | 169.9088 | 142.65 | 4.685 | 281.1 | 14.2125 | 22939.8 | 9724.758 | 93998 | 1367 | 995.2 | 472.3 | 182 | 188. |
| 7/20/2016 | | | 10.23 | 170.4713 | 142.02 | 4.6675 | 280.05 | 14.2125 | | | 87647 | 1362.5 | | | | |
| 7/20/2016 | | | 10.005 | 169.29 | 142.605 | 4.67 | 280.2 | 14.2125 | 22766.99 | | 93992 | | | | | |
| 7/20/2016 | | | 9.84 | | 140.94 | 4.68 | | 14.2125 | | | 87342 | | | | | |
| 7/20/2016 | | | 9.79 | | 140.85 | | | 14.2125 | | | 93566 | | | | | |
| 7/20/2016 | | | 9.8 | | 140.985 | | | 14.2125 | | | | | | | | |
| 7/20/2016 | | | | 169.5263 | 140.67 | 4.6825 | | 14.2125 | | | | | | | | |
| 7/20/2016 | | | 9.795 | | 141.3 | | | | | | | | | | | |
| | 13:10:00 | | | 164.2163 | 140.67 | | | | | 9764.084 | | | | | | |
| 7/20/2016 | | | | | 141.75 | | | | | | | | | | | |
| | 13:12:00 | | | | 141.21 | | | | | 9758.466 | | | | | | |
| 7/20/2016 | | | | | 141.21 | | | | | | | | | | | |
| | 13:14:00 | | 10.095 | | 140.13 | | | | | | | | | | | |
| | 13:15:00 | | 10.19 | | 141.255 | | | | | | | | | | | |
| 7/20/2016 | 13:16:00 | 26.97 | 10.15 | 168.1538 | 140.715 | 4.6725 | 280.35 | 14.2125 | 23299.25 | 9657.342 | 93601 | 1371.75 | 997.1 | 481.9 | 184.5 | 187 |
| | Average | 27.55 | 9.88 | 168.72 | 141.07 | 4.61 | 276.28 | 14.15 | 22763.04 | 9748.53 | 88368.05 | 1371.22 | 2 1000.98 | 482.92 | 2 187.72 | 190.1 |
| | | Protection and and and and and and and and and an | W/WWWWWWWW | | | | | 1 1. 1 1. | | | | R and | ne ne mananta minata manua | | | |
| uly 20, 2016 | b | Waste Flor | WS | | | | | | Air Flows | | | Temperate | ires | | | |

| July 20, 2016 | Waste Flo | WS | and the second | | | | | Air Flows | | | Temperatu | res | a parte de la compa | a di sha she | |
|---------------|-----------|----------|----------------|----------|----------|----------|----------|-----------|-----------|-----------|-----------|-----------|---------------------|---|----------|
| | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SprayDryer | Stack |
| Test1 | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | PV-236 | PV-209c | FT-260c | TE-240 | TE-241 | TE-203 | TE-204 | TE-258 |
| Max | 28.6 | 10.2 | 172.1 | 145.9 | 4.7 | 281.9 | 15.0 | 23299.3 | 9910.2 | 93998.0 | 1385.1 | 1007.6 | 491.2 | 192.0 | 192.4 |
| Min | 26.8 | 9.5 | 164.2 | 138.1 | 4.3 | 257.6 | 14.0 | 22324.6 | 9618.0 | 85431.0 | 1359.5 | 995.2 | 464.1 | 182.0 | 187.1 |
| Average | 27.5 | 9.9 | 168.7 | 141.1 | 4.6 | 276.3 | 14.2 | 22763.0 | 9748.5 | 88368.1 | 1371.2 | 1001.0 | 482.9 | 187.7 | 190.2 |
| Variance | 0.212873 | 0.031984 | 2.013136 | 4.818674 | 0.02241 | 80.4624 | 0.02464 | 50579.571 | 5631.785 | 5334513.4 | 34.92173 | 13.59168 | 40.10644 | 8.390179 | 3.383675 |
| | | · · · · | | | | | · . | | | | · · · · · | | | 1. A. | |
| | | | | | | | | | | | | | | | |

| 7/20/2016 12:21:00 -7:01 -4:64 314:375 22:9 98:32 8:1 40:06 11.7 8:71 1.4:8 98:13 27:7 7/20/2016 12:23:00 -2:3 -1:1.9 -8:64 3:4:475 22:2 3:8:66 7:4:7 3:1.2 8:66 7:4:7 3:1.2 8:66 7:4:7 3:1.2 3:1.6 6:67 7:4:7 3:1.2 3:1.6 6:67 7:4:4 8:84 1:1.2 8:66 2:2:7 7:7 </th <th>TEST 3</th> <th></th> <th>Incinerator</th> <th>SDA Inlet</th> <th>BH inlet</th> <th>BH dP</th> <th>со</th> <th>HCI</th> <th>CO2</th> <th>H2O</th> <th>тнс</th> <th>02</th> <th>Opacity</th> <th>SO2</th> <th>PAC</th> | TEST 3 | | Incinerator | SDA Inlet | BH inlet | BH dP | со | HCI | CO2 | H2O | тнс | 02 | Opacity | SO2 | PAC |
|--|-----------|----------|-------------|-----------|----------|----------|-----------|---------|---------|---------|-----------|--------|---------|--------|-------------------|
| 7/20/2016 122:100 17/2 11/2 | | | mmH2O | mmH2O | mmH2O | mmH2O | PPM | PPM | % | % | PPM | % | % | PPM | Lbs/h |
| 7707006 122200 -7.2 -31.9 -64.8 33.4 375 7.4.2 88.14 81.3 40.06 11.2 8.7.4 1.4.6 87.4 2.2.4 7/207016 12.2400 -6.6 -30.3 -66.65 33.5.2 21.3 86.66 7.94 40.06 11.4 8.86 1.46 87.4 22.5 7/207016 12.2500 -4.5 -34.55 34.625 31.1 87.5 7.85 40.06 11.7 8.84 1.5 854.4 22.5 7/207016 12.2800 -1.45 -7.4 56.05 30.1875 24.48 87.4 40.06 11.7 8.84 1.5 87.7 7/207016 12.2800 -1.4 -7.4 56.05 30.1875 2.44 85.1 8.12 40.06 11.5 8.71 1.5 8.72 2.12 7/207016 12.3000 -7.1 -5.07 3.85 30.857 2.24 85.7 8.00 60.15 1.1.8 8.8 1.42 867.7 7.7 7.7 8.1.2 1.2.8 8.1 8.8 1.8 | Date | Time | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205COF | AT-213A | AT-213B | AT-213C | AT-259COF | AT-261 | AT-263 | AT-264 | SC-PAC-FT |
| TAD/TODIG 12:23:00 -15:2 -15:6 -13:3 14:6 87:04 27:04 05:05 13:4 88:6 14:4 88:6 14:6 88:02 22:35 7/07/016 12:25:00 -10:6 -34:05 32:33:75 21:3 87:55 79:1 40:06 11:4 88:6 14:2 88:7 22:7 7/07/016 12:27:00 -48:5 -35:7 40:03:5 36:13:5 21:8 88:3:8 A0:06 11:7 8:71 32:2 7:7 7/07/016 12:21:00 -13:2 -7:7.5 24:1 85:18 8:12 40:06 11:1 8:54 1.5 8:84:4 22:8 8:81 A0:06 11:1 8:54 1.5 8:85 7:7 7:07/01:1 12:31:00 -18:2 -17:3 3:35 2:2 8:81:8 8:02 40:06 11:1 8:37 1.42 8:57 7:7 7:02:01 1:2:1 8:7 1.42 8:57 7:02:01 1:3:1 1:1:1 8:30 | | | | | | | | | | | | | | | 22.86375 |
| 7/20/2016 12:24:00 -6.6 -90.4 44:00.6 11.4 8.88 1.42 87:57 22.2 7/20/2016 12:25:00 -4.45 -84:25 31:43:75 71:3 87:55 71:8 40:06 11.4 8.84 1.5 85:44 22.2 7/20/2016 12:25:00 -4.45 -82:55 30:13:75 24:46 77:48 40:06 11.7 8.84 1.5 87:7 7/20/2016 12:28:00 -1.43 -22:45 50:05:2 30:13:75 24:16 87:44 87:4 1.5 87:7 1.5 87:2 22:2 88:81 81:2 40:06 11.1 8:4 1.5 89:07 72:2 72:2 72:2 72:2 72:2 88:3 8:02 40:06 11.1 8:3 1.42 89:77 72:7 72:2 72:2 72:2 8:3 1.42 89:77 72:2 1.5 8:3 1.42 80:75 72:2 1.22 8:34 8:0 40:06 11.4 8:9 1.42 89:57 72:7 72:2 72:2 72:2 72:2 <td></td> <td>22.24625</td> | | | | | | | | | | | | | | | 22.24625 |
| 7/20/2016 222500 -4.05 -84.05 84.252 21.3 37.55 7.95 40.06 11.4 8.84 1.5 88.44 22 7/20/2016 122700 -8.85 -8.85 75.5 23.37 77.5 78.8 40.06 11.7 8.71 8.84 22.77 7/20/2016 122700 -4.85 -8.75 23.8 8.83 8.04 40.06 11.7 8.71 32.8 8.77 7/20/2016 122300 -13.2 -77.5 52.55 23.0157 24.6 8.72.4 8.81 8.02 40.06 11.1 8.54 1.52 890.7 7/20/2016 123.300 -18.2 -74.8 5.95 33.05 22.2 8.81 8.02 40.05 11.7 8.87 1.42 85.7 7/20/2016 123.300 -7.5 -7.55 53.57 31.5 22.2 8.81 8.02 40.06 11.7 8.87 1.42 85.7 7/20/2016 123.300 -7.5 -5.97.852 38.57 21.9 84.1 40.06 11.7 | | | | | | | | | | | | | | | 22.8312 |
| 7/20/2016 12:26:00 -4:45 -78:35 56.812 22:37:5 7.13 77:55 7.83 40:06 11.7 8.84 1.5 88:44 22:5 7/20/2016 12:28:00 -1.45 -22:45 56:06:2 35:15:2 2.38 88:31 8:04 40:06 11.7 8.71 1.32 87:7 7/20/2016 12:20:00 -7.1 -97:5 75:57:55:23 30:1375 2.41 85:81 8:12 40:06 11.6 8.54 1.52 89:07 7/20/2016 12:31:00 -1.82 -4.25 7.77 32:5 7.71 71:7 32:5 7.71 71:7 71:2 8:31 8:02 40:06 11.1 8:31 1.42 89:67 7 7/20/2016 12:36:00 -73:5 -63:55 3:75 3:75 5:83:7 2:1 8:80 7.96 40:06 11.1 8:31 1.42 89:7 7 7 7:7 7:83:7 3:7 3:80:80 7.96 40:06 11.4 8:39 1.22 8:81:8 8:13 4:14 4:12 | | | | | | | | | | | | | | | 22.9612 |
| 7/70/2016 12/2700 9.85 -55. -69.037 34.46/25 21.9 87.7 78.3 40.06 11.7 8.89 1.35 65.44 22.7 7/70/2016 12.29800 -11.2 -27.55 75.5625 30.1875 24.6 87.24 81.32 40.06 11.1 85.44 13.2 890.7 7/70/2016 12.3900 -11.3 -21.75 75.875 30.0875 24.1 85.81 81.04 66 11.1 85.44 13.2 890.7 7/70/2016 12.3300 -4.8 -77.8 30.357 71.475 31.85 22.2 88.81 81.02 40.06 11.7 8.87 14.48 867.7 7/70/2016 12.3300 -4.5 -77.85 53.877.5 21.9 88.25 7.86 40.06 11.1 8.7 14.2 867.7 7/70/2016 12.3500 -7.15 -30.45 37.75 23.9 90.44 8.11 40.06 11.2 8.7 14.8 857.7 12.9 8.9 13.2 87.7 90.05 11.2 8.8 | | | | | | | | | | | | | | | 22.2462 22.652 |
| T/TO/2016 12.28400 1.45 -22.46 56.7125 23.8 88.32 80.4 40.06 11.6 83.4 11.5 87.7 T/TO/2016 12.3000 -71 -30.1 -56.737 340.1875 24.4 85.81 81.12 40.06 11.1 85.41 11.5 87.7 12.5 75.57.5525 350.877 22.4 85.97 84.40.06 11.1 85.81 11.4 85.81 14.8 865.5 27.7 77.70/2016 12.3300 -4.5 -77.477 31.5 22.2 88.85 7.75 40.06 11.1 8.95 14.8 865.7 77.70/2016 12.3300 -7.6 -32.65 -7.86.75 32.23 80.41 81.1 40.06 11.4 8.97 14.8 865.7 12.8 83.2 7.75 40.06 11.2 8.87 13.8 89.1 2.3 13.8 89.1 2.3 13.8 89.1 2.3 13.8 87.7 13.8 13.8 89.1 2.3 | | | | | | | | | | | | | | | 22.052 |
| 7/20/2016 12.2 37.5 75.523 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 30.1 57.733 57.8 40.06 11.1 8.8 11.3 8.1 11.1 8.8 11.3 8.1 11.3 8.3 11.3 8.3 11.3 8.3 11.1 8.3 11.3 8.3 | | | | | | | | | | | | | | | 23.0 |
| 7/20/2016 12:3000 -7.1 -8.01 -6.5737 30.01375 24.1 85.81 8.12 40.06 11.5 8.57 1.52 577.2 70.20 15.73 15.75 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 75.8 40.06 11.7 8.81 1.48 867.7 77.0 70.20 75.8 75.8 75.8 40.06 11.7 8.81 8.42 75.8 40.06 11.7 8.82 1.38 865.7 77.0 70.20 </td <td></td> <td>22.8962</td> | | | | | | | | | | | | | | | 22.8962 |
| PADQU06 1231400 -18.2 -42.6 -7.775 328.5 22.4 85.97 8 40.06 11.5 8.73 1.5 877.2 21.5 7/02/006 1233400 -9.25 -32.5 -7.475 318.5 22.2 88.81 8.02 40.06 11.7 8.87 14.4 867.7 7/02/016 1233400 -7.6 -32.65 -57.8675 315.7 21.3 88.25 7.86 40.06 11.1 8.97 14.8 87.7 14.8 87.7 14.8 87.7 14.8 87.7 14.8 87.7 14.8 12.8 842.9 12.8 842.9 12.8 842.9 12.8 842.9 12.8 842.9 12.8 842.9 12.8 842.9 12.8 842.9 12.8 842.9 12.8 842.9 12.8 12.8 14.8 851.6 22.7 12.8 843.9 12.8 12.8 14.8 851.6 22.7 12.2 12.8 12.8 14.8 | | | | | | | | | | | | | | | 22.6 |
| 7/20/2016 12:32:00 -4.8 -7.8 -5.80.5 330.62:5 22.5 86.86 7.97 40.06 12.1 8.81 1.48 966.5 22 7/20/2016 12:34:00 -4.55 -7.55 -55.875 331.5 22.4 88.69 7.05 40.06 11.5 8.92 1.32 862.9 22.3 7/20/2016 12:36:00 -7.6 -32.65 -57.86:7 330.87 22.3 90.41 8.11 40.06 12.1 8.1 1.32 862.9 22.3 89.1 2.3 40.06 11.2 8.21 1.40 8.51 1.23 89.31 2.3 90.41 8.11 40.06 11.2 8.81 1.3 89.1 7.3 40.06 11.2 8.31 4.8 85.6 7.2 7.7 7.00 7.7 -30.5 -66.0375 330 2.4 86.59 7.96 40.06 11.2 8.31 4.8 85.16 2.3 7.7 7.00 5.47.57 353.50.627 2.18 88.05 40.06 11.2 8.1 2.1 8.7 7.2 | | | | | | | | | | | | | | | 22.9937 |
| 7/20/2016 12:34:00 -4.55 -7.55 -55:847.5 311.5 22.4 88.69 79.5 40.06 11.7 8.88 1.48 865.7 7/20/2016 12:35:00 -7.6 -32.65 -7.862.5 34.75 22.9 90.41 81.1 40.06 11.1 8.7 1.26 886.7 22 7/20/2016 12:38:00 -5.15 -27.75 -64.837.5 332.2 2.53 90.44 8.21 40.06 11.2 8.51 83.1 2.83 1.84 861.6 2.2 7.75 -30.5 -66.037 330 23.4 66.53 7.56 40.06 11.2 8.83 1.48 851.6 2.2 7.77 7.00 1.2 8.93 1.48 851.6 2.2 7.77 7.00 1.2 8.93 1.48 851.6 2.2 7.77 7.00 1.2 8.93 1.48 851.6 2.2 7.77 7.00 1.2 8.93 7.87 40.06 11.2 8.93 7.87 40.06 11.4 9.44 1.48 853.7 2.2 7.77 <t< td=""><td></td><td>12:32:00</td><td></td><td></td><td>-58.05</td><td>339.0625</td><td></td><td></td><td>7.97</td><td>40.06</td><td></td><td></td><td>1.48</td><td>866.5</td><td>22.262</td></t<> | | 12:32:00 | | | -58.05 | 339.0625 | | | 7.97 | 40.06 | | | 1.48 | 866.5 | 22.262 |
| 7/20/2016 12:35:00 -7.6 -3.26.5 -57.86.2 345.75 21.9 88.25 7.86 40.06 11.5 8.92 1.32 88.29 1.32 88.29 1.32 88.29 1.32 88.29 1.32 88.29 1.32 88.29 1.32 88.21 40.06 11.4 8.59 1.36 89.45 2.2 7/20/2016 12:38:00 -7.75 -30.5 6.68.375 330 23.4 86.58 7.86 40.06 11.4 8.59 1.32 833 1.48 85.16 2.37 7/20/2016 12:4100 -4.45 -38.5 52.875 21.8 88.39 7.87 40.06 11.4 9.94 1.58 84.16 2.37 7/20/2016 12:43:00 -3.87 -3.76 33.55.57 22.58 87.89 7.88 40.06 11.7 88.1 1.21 85.64 2.37 7/20/2016 12:44:00 -3.87 3.76.5 33.96.52 20.9 87.36 80.06 11.5 8.91 1.21 85.47 2.38 3.38 85.4 3. | 7/20/2016 | 12:33:00 | -9.25 | -32.5 | -71.475 | 318.5 | 22.2 | 88.81 | 8.02 | 40.06 | 12.1 | 8.87 | 1.42 | 867.7 | 22.7 |
| 7/20/2016 12.365:00 0.35 > 2.195 -49.125 358.875 2.2.9 90.41 8.11 40.06 11.4 8.57 1.26 866 22 7/20/2016 12.38:00 -6.15 -29.75 -61.6875 338.25 2.6.3 90.48 82.1 40.06 11.2 8.58 1.32 89.1 2.2 7/20/2016 12.38:00 -6.15 -29.75 -61.6875 338.25 2.6.4 86.63 7.85 40.06 11.2 8.83 1.42 85.6 2.2 7.7 -7.75 -30.5 -66.0375 336.25 2.1.8 88.39 7.87 40.06 11.2 8.83 1.44 851.7 2.2 7/20/2016 12.42:00 -2.8 -2.62 -5.347 335.655 2.2.6 87.87 7.88 40.06 11.4 9.04 1.25 846.1 2.3 7/20/2016 12.44:00 -2.8 -7.55 -3.05 59.377 339.0625 2.09 87.35 8.06 40.06 11.8 8.71 1.38 89.1 33 85.3 2.1 </td <td>7/20/2016</td> <td>12:34:00</td> <td>-4.55</td> <td>-27.55</td> <td>-55.9875</td> <td>331.5</td> <td>22.4</td> <td>88.69</td> <td>7.95</td> <td>40.06</td> <td>11.7</td> <td>8.89</td> <td>1.48</td> <td>865.7</td> <td>22.49</td> | 7/20/2016 | 12:34:00 | -4.55 | -27.55 | -55.9875 | 331.5 | 22.4 | 88.69 | 7.95 | 40.06 | 11.7 | 8.89 | 1.48 | 865.7 | 22.49 |
| 7/20/2016 12:37:00 -10.85 -7.75 -44.8175 327.75 25.3 90.48 8.21 40.06 11.4 8.59 1.36 84.51 22.77 7/20/2016 12:38:00 -7.75 -30.5 -66.0375 330 23.4 86.58 7.96 40.06 11.2 8.72 1.42 89.31 23.7 7/20/2016 12:44:00 -7.75 -30.5 -66.0375 335.5225 22.0 86.63 7.85 40.06 11.2 8.83 1.48 851.6 22.7 7/20/2016 12:44:00 -2.8 -2.62 -5.34.75 335.5625 21.8 88.39 7.87 40.06 11.2 8.83 1.33 86.61 2 2.8 1.5 87.64 1.2 8.9 1.34 86.71 2 2.2 7.7 7.7 3.0 6.5 3.6 40.06 11.7 8.81 1.21 86.71 2.2 2.2 87.35 8.06 40.06 11.5 8.9 1.33 86.53 2.2 7.7 7.2 3.6 5.3 3.5 3.6 | 7/20/2016 | 12:35:00 | -7.6 | -32.65 | -57.8625 | 345.75 | 21.9 | 88.25 | 7.86 | 40.06 | 11.5 | 8.92 | 1.32 | 862.9 | 22.3112 |
| 7/20/2016 12/28/00 -6.15 -9.27 64.687 338.25 26.9 88.51 81.3 40.06 11.2 8.58 1.22 87.7 7/20/2016 12/39:00 -7.75 -30.5 -66.0375 330 23.4 86.98 7.96 40.06 11.2 8.72 1.42 87.4 2.44 87.4 2.24 7.97 40.06 11.2 8.73 1.46 85.37 2.2 7.97 40.06 11.2 8.83 1.46 85.37 2.2 7.97 40.06 11.4 9.04 1.5.5 87.47 2.2 7.97 40.06 11.4 9.04 1.2.5 87.47 7.8 40.06 11.4 9.04 1.2.5 87.45 7.2 7.97 7.97 40.06 11.8 8.91 1.2.3 87.7 7.7 7.97 7.97 7.97 7.97 7.97 7.97 8.4 40.06 11.8 8.97 1.3.3 87.7 7.7 8.7 7.9 40.06 11.5< | 7/20/2016 | 12:36:00 | 0.35 | -21.95 | -49.125 | 358.875 | 22.9 | 90.41 | 8.11 | 40.06 | 12.1 | 8.7 | 1.26 | 886 | 22.9775 |
| T/20/2016 12:39:00 -7.75 -80.5 -66:037 330 23.4 86.98 7.96 40.06 11.2 8.72 1.42 87.4 27.4 7/20/2016 12:44:00 -7.75 -31.5 59.25 322.562: 20.9 89.1 7.7 40.06 11.2 8.83 1.46 85.37 2 7/20/2016 12:44:00 -7.65 -31.7 59.25 322.562: 2.0.8 87.34 7.84 40.06 11.4 9.04 1.25 87.46 7.8 7/20/2016 12:44:00 -1.85 -30.6 51.1875 358.625 22.6 87.89 7.98 40.06 11.7 8.81 1.21 857.3 2.2 7/20/2016 12:44:50 -7.55 -30.05 -59.775 39.0625 2.9 86.48 7.9 40.06 11.3 9.0 1.33 854.3 2.2 7/20/2016 12:44:50 -7.55 -30.5 57.64625 325.8675 2.12 86.14 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>22.652</td></t<> | | | | | | | | | | | | | | | 22.652 |
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| 7/20/2016 12:53:00 -8.5 -31.7 -61.8 325.8125 25.6 85.21 7.92 40.06 11.5 8.83 1.3 862.3 22 7/20/2016 12:55:00 -12.1 -34.95 -70.35 325.9375 23.3 82.17 7.81 40.06 11.8 9.05 1.46 844.5 22.7 7/20/2016 12:56:00 -5.2 -52.4 -56.875 337.375 23.5 83.25 7.77 40.06 11.8 9.05 1.46 844.5 22.7 7/20/2016 12:56:00 -5.4 -56.875 337.375 23.5 83.07 7.67 40.06 11.5 9.09 1.46 827.8 22.7 7/20/2016 12:59:00 -5.45 -26.05 -57.6 300.5625 23.5 83.07 7.67 40.06 11.7 8.88 1.21 827.8 22.7 7/20/2016 13:00:00 -15.65 -47.75 -61.875 284.9375 25.4 80.25 7.91 40.06 11.7 8.77 1.38 86.21 22.7 7/20/ | 7/20/2016 | 12:51:00 | -7.2 | -29.1 | -61.5 | 345.25 | 23.5 | 86.62 | 7.67 | 40.06 | 12.1 | . 9.12 | 1.27 | 832.6 | 22.2462 |
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| 7/20/2016 12:56:00 -5.2 -25.4 -56:5875 337.375 23.5 83.25 7.77 40.06 12.4 9.14 1.52 83.4.4 22.4 7/20/2016 12:57:00 -8.45 -32.2 -58.9875 323.5 22.7 86.49 7.72 40.06 11.5 9.09 1.46 827.8 22. 7/20/2016 12:59:00 -5.45 -66.05 -57.6 300.5625 23.5 82.06 7.75 40.06 12.1 9.14 1.52 83.87 22. 7/20/2016 13:00:00 -15.65 -47.75 -61.875 264.9375 25.4 80.25 7.91 40.06 13.2 8.88 1.21 849.9 22. 7/20/2016 13:00:00 -11.1 -35.7 -67.5375 334.25 27.3 78.96 7.96 40.06 11.7 8.77 1.3 862.1 22. 7/20/2016 13:00:00 -11.75 -36.3 -68.4375 334.75 24.5 73.94 7.9 40.06 11.7 8.91 4.42 859.6 22. 22. | | | | | | | | | | | | | | | |
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| 7/20/2016 13:02:00 -25:95 -54:35 -73:6125 270:875 26.9 74.92 7.93 40.06 12.3 8.81 1.36 862.2 22. 7/20/2016 13:03:00 -11.75 -36.3 -68.4375 334.75 24.5 73.94 7.9 40.06 11.7 8.91 1.42 859.6 22. 7/20/2016 13:04:00 -29.15 -57.15 -80.325 267.1875 24 74.84 7.82 40.06 13 9.02 1.46 840 22. 7/20/2016 13:05:00 -9.65 -32.8 -73.7625 326.4375 26.3 76.79 7.79 40.06 11.7 9.04 1.46 839.8 22. 7/20/2016 13:06:00 -31.85 -58.1 -79.0875 273.0625 25.5 76.56 7.74 40.06 12.6 9.08 1.46 836.4 22. 7/20/2016 13:07:00 -7.25 -29.9 -61.9125 353.375 25.9 76.84 7.89 40.06 12.8 8.97 1.42 850.1 22. | | | | | | | | | | | | | | | |
| 7/20/2016 13:03:00 -11.75 -36.3 -68.4375 334.75 24.5 73.94 7.9 40.06 11.7 8.91 1.42 859.6 22. 7/20/2016 13:04:00 -29.15 -57.15 -80.325 267.1875 24 74.84 7.82 40.06 13 9.02 1.46 840 22. 7/20/2016 13:05:00 -9.65 -32.8 -73.7625 326.4375 26.3 76.79 7.79 40.06 11.7 9.04 1.46 839.8 22. 7/20/2016 13:06:00 -31.85 -58.1 -79.0875 273.0625 25.5 76.56 7.74 40.06 12.6 9.08 1.46 836.4 22. 7/20/2016 13:07:00 -7.25 -29.9 -61.9125 353.375 25.3 76.67 7.8 40.06 12.8 8.97 1.42 850.1 22. 7/20/2016 13:09:00 -11 -34.25 -70.9875 333.4375 27 76.25 7.96 40.06 11.5 8.8 1.3 862.8 22. <tr< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></tr<> | | | | | | | | | | | | | | | |
| 7/20/201613:04:00-29.15-57.15-80.325267.18752474.847.8240.06139.021.4684022.7/20/201613:05:00-9.65-32.8-73.7625326.437526.376.797.7940.0611.79.041.46839.822.7/20/201613:06:00-31.85-58.1-79.0875273.062525.576.567.7440.0612.69.081.46836.422.7/20/201613:07:00-7.25-29.9-61.9125353.37525.376.677.840.0612.19.021.21844.222.7/20/201613:08:00-31.1-61.35-80.175260.937525.976.847.8940.0611.58.81.3862.822.7/20/201613:09:00-11-34.25-70.987533.43752776.257.9640.0611.58.81.3862.822.7/20/201613:10:00-31.15-57.7-81.825270.62525.974.317.8740.0612.98.921.42851.22.27/20/201613:11:00-9.2-33.55-64.35337.687525.574.137.8240.0612.99.011.46838.722.7/20/201613:11:00-27.85-56.2-77.8125273.62526.375.647.8240.0612.99.011.46838.722.7/20/201613:1 | | | | | | | | | | | | | | | |
| 7/20/2016 13:05:00 -9.65 -32.8 -73.7625 326.4375 26.3 76.79 7.79 40.06 11.7 9.04 1.46 839.8 22. 7/20/2016 13:06:00 -31.85 -58.1 -79.0875 273.0625 25.5 76.56 7.74 40.06 12.6 9.08 1.46 836.4 22. 7/20/2016 13:07:00 -7.25 -29.9 -61.9125 353.375 25.3 76.67 7.8 40.06 12.1 9.02 1.21 844.2 22. 7/20/2016 13:08:00 -31.1 -61.35 -80.175 260.9375 25.9 76.84 7.89 40.06 12.8 8.97 1.42 850.1 22. 7/20/2016 13:09:00 -11 -34.25 -70.9875 333.4375 27 76.25 7.96 40.06 11.5 8.8 1.3 862.8 22. 7/20/2016 13:1:00 -9.2 -33.55 -64.35 337.6875 25.5 74.13 7.82 40.06 12.3 8.98 1.46 843 22. < | | | | | | | | | | | | | | | |
| 7/20/2016 13:06:00 -31.85 -58.1 -79.0875 273.0625 25.5 76.56 7.74 40.06 12.6 9.08 1.46 836.4 22. 7/20/2016 13:07:00 -7.25 -29.9 -61.9125 353.375 25.3 76.67 7.8 40.06 12.1 9.02 1.21 844.2 22. 7/20/2016 13:08:00 -31.1 -61.35 -80.175 260.9375 25.9 76.84 7.89 40.06 12.8 8.97 1.42 850.1 22. 7/20/2016 13:09:00 -11 -34.25 -70.9875 333.4375 27 76.25 7.96 40.06 11.5 8.8 1.3 862.8 22. 7/20/2016 13:10:00 -31.15 -57.7 -81.825 270.625 25.9 74.13 7.87 40.06 12.3 8.98 1.46 843 22. 7/20/2016 13:11:00 -9.2 -33.55 -64.35 337.6875 25.5 74.13 7.82 40.06 12.3 8.98 1.46 843. 22. <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | | | | | | | | | | | | | | | |
| 7/20/2016 13:07:00 -7.25 -29.9 -61.9125 353.375 25.3 76.67 7.8 40.06 12.1 9.02 1.21 844.2 22. 7/20/2016 13:08:00 -31.1 -61.35 -80.175 260.9375 25.9 76.84 7.89 40.06 12.8 8.97 1.42 850.1 22. 7/20/2016 13:09:00 -11 -34.25 -70.9875 333.4375 27 76.25 7.96 40.06 11.5 8.8 1.3 862.8 22. 7/20/2016 13:10:00 -31.15 -57.7 -81.825 270.625 25.9 74.31 7.87 40.06 12.9 8.92 1.42 851.2 27. 7/20/2016 13:11:00 -9.2 -33.55 -64.35 337.6875 25.5 74.13 7.82 40.06 12.3 8.98 1.46 843 22. 7/20/2016 13:12:00 -27.85 -56.2 -77.8125 273.625 26.3 75.64 7.82 40.06 12.9 9.01 1.46 838.7 22. <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | | | | | | | | | | | | | | | |
| 7/20/2016 13:09:00 -11 -34.25 -70.9875 333.4375 27 76.25 7.96 40.06 11.5 8.8 1.3 862.8 22. 7/20/2016 13:10:00 -31.15 -57.7 -81.825 270.625 25.9 74.31 7.87 40.06 12.9 8.92 1.42 851.2 27 7/20/2016 13:11:00 -9.2 -33.55 -64.35 337.6875 25.5 74.13 7.82 40.06 12.3 8.98 1.46 843 22 7/20/2016 13:12:00 -27.85 -56.2 -77.8125 273.625 26.3 75.64 7.82 40.06 12.9 9.01 1.46 838.7 22. 7/20/2016 13:13:00 -8.75 -34.25 -62.325 328.9375 26 76 7.8 40.06 12 8.94 1.46 838.7 7/20/2016 13:14:00 -28.75 -50.55 -88.4625 298.0625 25.4 74.09 7.73 40.06 12.6 9.02 1.46 833.4 22 7/20/2016 <td>7/20/2016</td> <td>13:07:00</td> <td>-7.25</td> <td>-29.9</td> <td>-61.9125</td> <td>353.375</td> <td></td> <td></td> <td>7.8</td> <td>40.06</td> <td>12.1</td> <td>9.02</td> <td>1.21</td> <td>844.2</td> <td>22.9287</td> | 7/20/2016 | 13:07:00 | -7.25 | -29.9 | -61.9125 | 353.375 | | | 7.8 | 40.06 | 12.1 | 9.02 | 1.21 | 844.2 | 22.9287 |
| 7/20/2016 13:10:00 -31.15 -57.7 -81.825 270.625 25.9 74.31 7.87 40.06 12.9 8.92 1.42 851.2 2 7/20/2016 13:11:00 -9.2 -33.55 -64.35 337.6875 25.5 74.13 7.82 40.06 12.3 8.98 1.46 843 22 7/20/2016 13:12:00 -27.85 -56.2 -77.8125 273.625 26.3 75.64 7.82 40.06 12.9 9.01 1.46 838.7 22. 7/20/2016 13:13:00 -8.75 -34.25 -62.325 328.9375 26 76 7.8 40.06 12 8.94 1.46 838.7 7/20/2016 13:14:00 -28.75 -50.55 -88.4625 298.0625 25.4 74.09 7.73 40.06 12.6 9.02 1.46 833.4 22 7/20/2016 13:15:00 -7.25 -30.7 -61.6875 352.875 26.5 74.53 7.88 40.06 12.6 8.91 1.17 850.1 7/20/2016 13:1 | | | -31.1 | -61.35 | -80.175 | 260.9375 | 25.9 | 76.84 | 7.89 | 40.06 | 12.8 | 8 8.97 | 1.42 | 850.1 | 22.9937 |
| 7/20/201613:11:00-9.2-33.55-64.35337.687525.574.137.8240.0612.38.981.46843227/20/201613:12:00-27.85-56.2-77.8125273.62526.375.647.8240.0612.99.011.46838.722.7/20/201613:13:00-8.75-34.25-62.325328.937526767.840.06128.941.46838.77/20/201613:14:00-28.75-50.55-88.4625298.062525.474.097.7340.0612.69.021.46833.4227/20/201613:15:00-7.25-30.7-61.6875352.87526.574.537.8840.0612.68.911.17850.17/20/201613:16:00-31.25-55.95-94.3875286.62526.874.397.8840.0613.68.871.36855.622 | | | | | | | | | | 40.06 | | | | | |
| 7/20/201613:12:00-27.85-56.2-77.8125273.62526.375.647.8240.0612.99.011.46838.722.7/20/201613:13:00-8.75-34.25-62.325328.937526767.840.06128.941.46838.77/20/201613:14:00-28.75-50.55-88.4625298.062525.474.097.7340.0612.69.021.46833.4227/20/201613:15:00-7.25-30.7-61.6875352.87526.574.537.8840.0612.68.911.17850.17/20/201613:16:00-31.25-55.95-94.3875286.62526.874.397.8840.0613.68.871.36855.622 | | | | | | | | | | | | | | | |
| 7/20/2016 13:13:00 -8.75 -34.25 -62.325 328.9375 26 76 7.8 40.06 12 8.94 1.46 838.7 7/20/2016 13:14:00 -28.75 -50.55 -88.4625 298.0625 25.4 74.09 7.73 40.06 12.6 9.02 1.46 833.4 22 7/20/2016 13:15:00 -7.25 -30.7 -61.6875 352.875 26.5 74.53 7.88 40.06 12.6 8.91 1.17 850.1 7/20/2016 13:16:00 -31.25 -55.95 -94.3875 286.625 26.8 74.39 7.88 40.06 13.6 8.87 1.36 855.6 22 | | | | | | | | | | | | | | | |
| 7/20/2016 13:14:00 -28.75 -50.55 -88.4625 298.0625 25.4 74.09 7.73 40.06 12.6 9.02 1.46 833.4 22 7/20/2016 13:15:00 -7.25 -30.7 -61.6875 352.875 26.5 74.53 7.88 40.06 12.6 8.91 1.17 850.1 7/20/2016 13:16:00 -31.25 -55.95 -94.3875 286.625 26.8 74.39 7.88 40.06 13.6 8.87 1.36 855.6 22 | | | | | | | | | | | | | | | |
| 7/20/2016 13:15:00 -7.25 -30.7 -61.6875 352.875 26.5 74.53 7.88 40.06 12.6 8.91 1.17 850.1 7/20/2016 13:16:00 -31.25 -55.95 -94.3875 286.625 26.8 74.39 7.88 40.06 13.6 8.87 1.36 855.6 22 | | | | | | | | | | | | | | | |
| 7/20/2016 13:16:00 -31.25 -55.95 -94.3875 286.625 26.8 74.39 7.88 40.06 13.6 8.87 1.36 855.6 22 | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| Average -11.67 -35.80 -66.58 325.02 23.86 83.58 7.90 40.06 11.91 8.89 1.39 856.58 | //20/2016 | | | | | | | | | | | | | | |
| | | Average | -11.67 | -35.80 | -66.58 | 325.02 | 23.86 | 5 83.58 | 7.90 | 40.06 | 11.91 | 8.89 | 1.39 | 856.58 | 22.6 |

| July 20, 2016 | Pressures | 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - | 1111 | i i fa da sel | Analyzers | | | | | | 1. S. S. | 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - | Flows |
|---------------|-------------|---|-----------|---------------|-----------|----------|----------|----------|---------|----------|----------|---|-----------|
| | Incinerator | SDA Inlet | SD Outlet | Baghouse | CO | HCI | CO2 | H2O | тнс | 02 | Opacity | SO2 | PACFlow |
| Test1 | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC-FT |
| Max | 0.4 | -22.0 | -49.1 | 359.6 | 27.3 | 90.5 | 8.2 | 40.1 | 13.6 | 9.2 | 1.5 | 894.5 | 23.1 |
| Min | -31.9 | -61.4 | -94.4 | 260.9 | 20.4 | 73.9 | 7.7 | 40.1 | 10.8 | 8.5 | 1.2 | 827.8 | 22.2 |
| Average | -11.7 | -35.8 | -66.6 | 325.0 | 23.9 | 83.6 | 7.9 | 40.1 | 11.9 | 8.9 | 1.4 | 856.6 | 22.7 |
| Variance | 72.5371 | 102.0737 | 100.2218 | 638.7544 | 3.599519 | 30.27618 | 0.016418 | 1.85E-27 | 0.37275 | 0.025702 | 0.009351 | 308.1166 | 0.0850191 |

| TEST 4 | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | | | Stack |
|--|--|------------------|-------------------------|---------------------------------|--------------------|--------------------|--------------------|-----------------------------|----------------------|----------------------|----------------|----------------------|----------------|----------------|-------------------|--------------|
| | | LPM | LPM | LPM | LPM | LPM | SCFM | LPM | m3/h | m3/h | m3/h | Degrees C | Degrees C | Degrees C | Degrees C | Degrees C |
| AND ADDRESS OF TAXABLE PARTY OF TAXABLE PARTY. | Time | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | PV-236 | PV-209 | FT-260C | TE-240 | TE-241 | TE-203 | TE-204 | TE-258 |
| 7/20/2016 | 13:38:00 | 27.15 | 9.95 | | 140.31 | 5.5 | 330 | 14.2125 | 22504.31 | 9578.69 | 88508 | 1377.875 | 993 | 480.9 | 185.5 | 188. |
| 7/20/2016 | 13:39:00 | 27.42 | 10.31 | 170.145 | 140.985 | 5.57125 | 334.275 | 14.2125 | 22151.77 | 9578.69 | 87151 | 1383.625 | 992.2 | 479.9 | 185 | 188. |
| 7/20/2016 | 13:40:00 | 27.465 | 9.855 | 168.39 | 140.04 | 6.13625 | 368.175 | 14.2125 | 23036.58 | 9691.05 | 88892 | 1374.375 | 993.6 | 481.6 | 184.5 | 187. |
| 7/20/2016 | 13:41:00 | 27.39 | 9.98 | | 139.995 | 4.60875 | 276.525 | 14.2125 | 22497.4 | 9589.926 | 88187 | 1368.125 | 993 | 482 | 185 | 187. |
| 7/20/2016 | 13:42:00 | 27.33 | 9.845 | | 138.78 | 4.895 | 293.7 | 14.2125 | 22946.71 | 9707.904 | 88060 | 1361.375 | 994.2 | 482.9 | 185 | 187. |
| 7/20/2016 7/20/2016 | 13:43:00 13:44:00 | 27.63 27.42 | 9.755 9.765 | 171.7538 169.2 | 139.365 138.285 | 4.95125 4.72375 | 297.075 283.425 | 14.2125 14.2125 | 22504.31 22766.99 | 9483.184 9629.252 | 87685 88322 | 1365.125 1359.375 | 992.7 993.2 | 481.9 482.8 | 185 185.5 | 188. 188. |
| 7/20/2016 | 13:44:00 | 27.42 | | | 138.285 | 4.92875 | 205.425 | 14.2125 | 22766.99 | 9629.252 | 87572 | 1361.875 | 995.2 994.4 | 482.6 | 185.5 | 188. |
| 7/20/2016 | 13:45:00 | 27.53 | | | 138.645 | 5.65625 | 339.375 | 14.2125 | 22587.26 | 9584.308 | 87372 | 1357.5 | 991.6 | 482.0 | 185.5 | 188. |
| 7/20/2016 | 13:47:00 | 27.36 | | | 138.049 | 7.24375 | 434.625 | 14.2125 | 22387.20 | 9477.566 | 87443 | 1364.875 | 995.6 | 482.6 | 185.5 | 180. |
| 7/20/2016 | 13:48:00 | 26.91 | 10.105 | | 139.95 | 5.1475 | 308.85 | 14.2125 | 22856.85 | 9629.252 | 88217 | 1360.125 | 992.7 | 484.3 | 185.5 | 18 |
| 7/20/2016 | 13:49:00 | 27.375 | 10.15 | | 141.165 | 4.74375 | 284.625 | 14.2125 | 22766.99 | 9528.128 | 86942 | 1364.125 | 994 | 484.9 | 185.5 | 18 |
| 7/20/2016 | 13:50:00 | 27.075 | 9.9 | | 140.49 | 5.76 | 345.6 | 14.2125 | 23036.58 | 9640.488 | 88444 | 1352.875 | 992.1 | 486.8 | 186 | 188. |
| 7/20/2016 | 13:51:00 | 27.36 | 10.07 | 167.9625 | 141.03 | 5.5625 | 333.75 | 14.2125 | 22684.04 | 9640.488 | 88348 | 1359.5 | 992.8 | 486.3 | 186 | 188. |
| 7/20/2016 | 13:52:00 | 27.585 | 9.995 | 168.0075 | 139.86 | 4.27 | 256.2 | 14.2125 | 22594.17 | 9646.106 | 88655 | 1359.375 | 994.3 | 487 | 186 | 188. |
| 7/20/2016 | 13:53:00 | 27.315 | 9.615 | 170.4262 | 139.275 | 4.5025 | 270.15 | 14.2125 | 22414.45 | 9539.364 | 87061 | 1360.75 | 991.8 | 485.8 | 186 | 188. |
| 7/20/2016 | 13:54:00 | 27.315 | 9.6 | 166.8262 | 138.735 | 5.14375 | 308.625 | 14.2125 | 22587.26 | 9634.87 | 88175 | 1355.75 | 995.9 | 487.2 | 186.5 | 188. |
| 7/20/2016 | 13:55:00 | 26.565 | 9.83 | 169.38 | 138.69 | 4.555 | 273.3 | 14.2125 | 22684.04 | 9533.746 | 86888 | 1362.625 | 995 | 485.8 | 186.5 | 188. |
| 7/20/2016 | 13:56:00 | 27.285 | 9.945 | 170.4713 | 138.87 | 4.55125 | 273.075 | 14.2125 | 23119.52 | 9646.106 | 90048 | 1356.75 | 993.7 | 487.9 | 187 | 188. |
| 7/20/2016 | 13:57:00 | 27.435 | 9.945 | | 139.41 | 4.9025 | 294.15 | 14.2125 | 22587.26 | 9646.106 | 87938 | 1356 | 992.2 | 487.4 | 187 | 188. |
| 7/20/2016 | 13:58:00 | 27.03 | 9.885 | | 138.69 | 5.27375 | 316.425 | 14.2125 | 22766.99 | 9646.106 | 88233 | 1349.125 | 995.1 | 488.8 | 187.5 | 188. |
| 7/20/2016 | 13:59:00 | 27.705 | 9.845 | | 139.95 | 4.955 | 297.3 | 14.2125 | 22421.36 | 9657.342 | 87195 | 1357 | 993.4 | 487.2 | 187.5 | 188. |
| 7/20/2016 | 14:00:00 | 27.39 | 10.23 | | 139.86 | 4.64375 | 278.625 | 14.2125 | 22587.26 | 9657.342 | 88983 | 1357.125 | 995.3 | 487.7 | 187.5 | 189. |
| 7/20/2016 | 14:01:00 | 27.24 | 10.055 | | 139.905 | 5.00375 | 300.225 | 14.2125 | 22856.85 | 9533.746 | 89808 | 1360.125 | 994.5 | 487.1 | 187.5 | 188. |
| 7/20/2016 | 14:02:00 | 27.15 | 9.725 | | 139.95 | 5.0025 | 300.15 | 14.2125 | 22504.31 | 9522.51 | 87818 | 1360.875 | 993.7 | 488.1 | 187.5 | 188. |
| 7/20/2016 | 14:03:00 | 27.345 | 10.045 | | 139.185 | 6.455 | 387.3 | 14.2125 | 22594.17 | 9522.51 | 92906 | 1365.75 | 997.5 | 487.4 | 187 | 188. |
| 7/20/2016 | 14:04:00 | 27.435 | 10.225 | | 139.23 | 6.99 | 419.4 | 14.2125 | 22856.85 | 9623.634 | 88412 | 1358.375 | 997 | 489.9 | 187.5 | 188. |
| 7/20/2016 | 14:05:00 | 27.12 | 9.815 | | | 7.91 | 474.6 | | 23036.58 | 9516.892 | 93154 | 1361.75 | 996 | 489.1 | 187.5 | 188. |
| 7/20/2016 | 14:06:00 | 27.345 | 9.95 | | 138.87 | 7.9125 | 474.75 | | 22766.99 | 9640.488 | 88021 | 1355.5 | 994 | 488.4 | 188 | 188. |
| 7/20/2016 | 14:07:00 | 27.135 | 9.89 | | 138.87 | 7.91 | 474.6 | | 22863.76 | | 93642 | 1360.25 | 994.9 | 482.5 | 187 | 189. |
| 7/20/2016 | 14:08:00 | 27.39 | 9.805 | | 138.825 | 7.25875 | 435.525 | | 22684.04 | | 87958 | 1354.5 | 994.6 | 480.2 | 186 | 188. |
| | 14:09:00 | 27.24 | 9.81 | | 138.285 | 7.91 | 474.6 | | 23119.52 | | 93073 | 1359.75 | | 477.2 | 184.5 | |
| | 14:10:00 | 27.345 | 10.01 | | 138.825 | 6.43625 | 386.175 | | 22766.99 | 9516.892 | 87831 | 1358.875 | 994.7 | 477.5 | 184 | 188. |
| 7/20/2016 | | 27.405 | 9.87 | 132.48 | 139.545 | 7.73 | 463.8 | | 23389.11 | | 93042 | 1362.125 | | 475.7 | 183 | 187. |
| 7/20/2016 | | 27.57 | 9.975 | 169.245 | 139.41 | 8.3875 | 503.25 | | 22684.04 | 9618.016 | 88174 | 1358 | | 479.1 | 182.5 | |
| 7/20/2016 | | 27.135 | 9.8 | | 139.32 | 7.9075 | 474.45 | | 23126.44 | 9618.016 | 92852 | 1358.75 | | 484.4 | 183 | |
| 7/20/2016 | | 27.405 | 9.885 | 166.635 | | 5.37375 | 322.425 | | 22594.17 | | 88729 | 1358 | | 482.9 | 184 | |
| 7/20/2016 | | 27 | 9.58 | | 138.24 | 6.4775 | 388.65 | | 23119.52 | | 91909 | 1358 | | 484.6 | 183.5 | |
| 7/20/2016 7/20/2016 | | 27.27 | 9.88 | 171.4725 169.245 | 139.545 137.61 | 6.01125 | 360.675 399.075 | | 22241.64 23478.97 | 9511.274 9640.488 | 87696 | 1357.875 | | 487.3 | 184.5 | |
| 7/20/2016 | | 27.195 | 9.785 9.705 | | 138.69 | 6.65125 5.265 | 315.9 | | 22504.31 | 9522.51 | 89964 87458 | 1359.125 1361.125 | | 488.8 489.7 | 185 185.5 | |
| 7/20/2016 | | 27.15 27.6 | | 169.0557 | | 5.60375 | 336.225 | | 23396.02 | | 90712 | 1359.25 | | 489.7 | 185.5 | |
| 7/20/2016 | | 27.195 | | 170.4262 | | 5.23875 | 314.325 | | 22594.17 | | 88229 | 1356.875 | | 489.9 | 185.5 | |
| 7/20/2016 | | | 9.925 | 169.29 | 137.79 | 6.87875 | 412.725 | | 23299.25 | | 90652 | 1353.375 | | 490.3 | 180.5 | 187. |
| 7/20/2016 | | | | 170.4713 | | | | | 22684.04 | | 87806 | 1353.373 | | 490.8 | 188 | |
| 7/20/2016 | | | | 169.9537 | | | | | | | | 1351.875 | | | 187.5 | |
| 7/20/2016 | | | | 171.4725 | | | | | | 9528.128 | 86789 | 1354.25 | | | 187.5 | |
| 7/20/2016 | | | | | | | | | | | 88175 | 1353.125 | | | 187.5 | |
| 7/20/2016 | | | | 169.6162 | | 6.49 | 389.4 | | | | 86219 | 1358.25 | | 488.6 | 187.5 | |
| 7/20/2016 | | | | | | | | | | | 90169 | 1356.875 | | | 187.5 | |
| 7/20/2016 | | | | | | 5.9075 | 354.45 | | | 9550.6 | 87983 | 1357.5 | | | 187.5 | |
| 7/20/2016 | | | | 169.9988 | | | | | | | 89598 | 1353.875 | | | 187.5 | |
| 7/20/2016 | | | | 170.6175 | | | | | | | 88067 | 1354.625 | | | 188 | |
| 7/20/2016 | | | | | | | | | | 9657.342 | 88864 | 1353.875 | | | 188 | |
| 7/20/2016 | | | | 169.6725 | | | | | | | 88313 | 1356 | | | 188 | |
| 7/20/2016 | | | | 170.3812 | | | | | | | 87874 | 1354.5 | | | 188 | |
| 7/20/2016 | | | | | | | | | | 9443.858 | 86026 | 1357.875 | | | 188 | |
| 7/20/2016 | 14:35:00 | | | 169.9537 | 137.52 | 7.48 | | | 22946.71 | 9657.342 | 89143 | 1354.75 | 996.3 | 488.8 | 187.5 | 188 |
| 7/20/2016 | 14:36:00 | 27.3 | 10.01 | 170.8537 | 138.78 | 5.335 | 320.1 | 14.2125 | 22594.17 | 9522.51 | 87292 | 1358 | 996.9 | 489.2 | 188 | 189 |
| 7/20/2016 | 14:37:00 | 27.255 | 9.97 | 169.5712 | 138.465 | 5.81375 | 348.825 | 14.2125 | 22953.63 | 9623.634 | 88470 | 1352 | 996.2 | 490.8 | 188 | 189 |
| 7/20/2016 | 14:38:00 | 27.465 | | 170.3812 | | 7.59625 | 455.775 | 14.2125 | | | 87191 | 1358.25 | 995.9 | 490.1 | 188 | 189 |
| | Average | 27.31 | 9.89 | 168.11 | 139.02 | 5.89 | 353.49 | 14.21 | 22745.34 | 9595.54 | 88752.54 | 1359.05 | 994.57 | 486.21 | 186.33 | 188.1 |
| July 20, 2016 | | Waste Flo | WS | kapatén k | | | | | Air Flows | **** | | Temperatu | ires | 1 | | |
| | | Rich | | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SprayDryer | Stack |
| Test1 | | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | PV-236 | PV-209c | FT-260c | TE-240 | TE-241 | TE-203 | TE-204 | TE-258 |
| Max | ., | 27.7 | สุขารสาวารสาวอาการสาวาร | formation and the second second | | ***** | | งรุ่งเหลือสมาร์สองสามาร์สอง | 23479.0 | | 93642.0 | 1383.6 | | | 188.0 | |
| la contra c | , | 26.6 | L | | | 4.3 | | + | 22151.8 | | 86026.0 | 1349.1 | | | 182.5 | 1 |
| Min | | | | | | | 1 | 1 | | 1 | , | | , | 1 | | |
| | and the second | | | 168.1 | 139.0 | 5.9 | 353.5 | 14.2 | 22745 3 | 9595.5 | 88752 5 | 1359 1 | 994 6 | 486.2 | 186.3 | 188. |
| Min Average Variance | | 27.3 0.038874 | 9.9 | | | | | | | | | 1359.1 34.19238 | | | 186.3 2.249044 | |

| TEST 4 | | Incinerator | | | | | HCI | | H2O | тнс | 02 | Opacity | SO2 | PAC |
|--|----------------------|------------------|--|---|--|--------------|----------------|--------------|----------------|------------------------------|---|---------------------------------------|---------|-------------------|
| | | mmH2O | mmH2O | Inconvertex community and | and the second | PPM | PPM | % | % | PPM | % | % | PPM | Lbs/h |
| TAXABLE PARTY AND A DESCRIPTION OF THE PARTY | Time | PT-242A | the construction of the second s | Lange and the second | | AT-205COR | | | AT-213C | AT-259COR | AND THE OWNER | AT-263 | AT-264 | SC-PAC-FT |
| 7/20/2016 | 13:38:00 | -10.05 | -32.55 | -81.4875 | 347.25 | 34.9 | 67.41 | 7.62 | 40.06 | | 9.14 | | | 22.1812 |
| 7/20/2016 | 13:39:00 | -6.9 | -28.1 | -64.8 | 360 | 37.6 | 66.82 | 7.86 | 40.06 | | 9 | | | 22.42 |
| 7/20/2016 7/20/2016 | 13:40:00 | -15.9 | -39.55 | -80.7375 | 329 343.125 | 38.7 | 66.24 | 7.94 | 40.06 | | 8.94 | | | 22.863 |
| 7/20/2016 | 13:41:00 13:42:00 | -10.85 -16.05 | -33.95 -39.3 | -69.825 -77.85 | 343.125 | 38.5 27.2 | 63.14 62.46 | 7.93 7.8 | 40.06 40.06 | | 8.83 9.01 | | | 22.6037 22.652 |
| 7/20/2016 | 13:42:00 | -10.05 -9.1 | -39.5 | -70.95 | 345.625 | 25.2 | 63.71 | 7.8 | 40.06 | | 9.01 | | | 22.5062 |
| 7/20/2016 | 13:43:00 | -9.1 | -31.45 | -69.7125 | 325.125 | 25.2 | 67.91 | 7.8 | 40.06 | | 9.02 | | | 22.3082 |
| 7/20/2016 | 13:45:00 | -5.65 | -27.8 | -60.9375 | 336.3125 | 25.2 | 68.19 | 7.7 | 40.06 | | 9.02 | | | 22.3437 |
| 7/20/2016 | 13:46:00 | -9.15 | -31.7 | -71.3625 | 349.0625 | 9.5 | 29.44 | 2.46 | 40.06 | | 11.46 | · · · · · · · · · · · · · · · · · · · | 319.2 | 22.2462 |
| 7/20/2016 | 13:47:00 | -4.75 | -23.75 | -65.8875 | 359.5625 | 7.8 | 27.41 | 1.88 | 40.06 | | 12.28 | 3 | 225.5 | 22.327 |
| 7/20/2016 | 13:48:00 | -14.2 | -39.2 | -77.1375 | 329.8125 | 27.3 | 73.44 | 6.74 | 40.06 | | 10.12 | Opacity | 718.8 | 22.8962 |
| 7/20/2016 | 13:49:00 | -9.3 | -31.75 | -63.975 | 341.0625 | 29 | 76.41 | 7.74 | 40.06 | | 9.01 | Daily Calibration | 853.9 | 22.97 |
| 7/20/2016 | 13:50:00 | -14.05 | -37.5 | -69.45 | 327.75 | 28 | 74.31 | 7.82 | 40.06 | | 9.11 | | 864.3 | 22.522 |
| 7/20/2016 | 13:51:00 | -10.5 | -33.7 | -64.9875 | 341.8125 | 26.3 | 72.59 | 7.77 | 40.06 | | 9.12 | 1 | 844.1 | 22.7012 |
| 7/20/2016 | 13:52:00 | -13.7 | -36.95 | -74.7375 | 321.0625 | 27.4 | 73.62 | 7.78 | 40.06 | 11.9 | 9.09 | 1.31 | . 845.3 | 22.262 |
| 7/20/2016 | 13:53:00 | -8.4 | -30.25 | -64.8375 | 335.5625 | 27.8 | 72.68 | 7.65 | 40.06 | 12.2 | 9.18 | 1.36 | 840 | 22.912 |
| 7/20/2016 | 13:54:00 | -10.3 | -31.8 | -71.7375 | 350.1875 | 26.4 | 72.88 | 7.78 | 40.06 | 11.7 | 9.15 | 1.22 | 847.6 | 22.782 |
| 7/20/2016 | 13:55:00 | -5.9 | -26.45 | -61.6875 | 359.125 | 25.7 | 73.22 | 7.82 | 40.06 | 11.9 | 9.07 | 1.12 | 851.6 | 22.4 |
| 7/20/2016 | 13:56:00 | -14.65 | -38.2 | -72.225 | 332.25 | 25.8 | 73.29 | 7.88 | 40.06 | 11.3 | 8.98 | 1.2 | 862.3 | 22.7987 |
| 7/20/2016 | 13:57:00 | -11.05 | -37 | | 325.375 | 25.6 | 72.62 | 7.83 | 40.06 | | 9.01 | | | 22.522 |
| 7/20/2016 | 13:58:00 | -13.1 | | -65.175 | 331.25 | 24 | 72.45 | 7.75 | 40.06 | | 9.16 | | | 22.652 |
| 7/20/2016 | 13:59:00 | -9.3 | | | 296.1875 | 24 | 73.64 | 7.76 | 40.06 | | 9.18 | | | 22.2137 |
| 7/20/2016 | 14:00:00 | -10.85 | -35.15 | -68.025 | 323 | 24.4 | 75.35 | 7.76 | 40.06 | | 9.07 | | | 23.042 |
| 7/20/2016 | 14:01:00 | -12.75 | -42.9 | -68.475 | 293.5 | 28.4 | 74.07 | 7.68 | 40.06 | | 9.15 | | | 22.94 |
| 7/20/2016 | 14:02:00 | -7.8 | -30.45 | -63.5625 | 347 | 29.7 | 74.01 | 7.78 | 40.06 | | 9.2 | | | 22.262 |
| 7/20/2016 | 14:03:00 | -21.85 | -52.6 | | 287.375 | 27.7 | | 7.94 | 40.06 | | 8.9 | | | |
| 7/20/2016 | 14:04:00 | -12.35 | -36.15 | -66.15 | 332.8125 | 30.1 | 72.84 | 7.99 | 40.06 | | 8.83 | | | 22.993 |
| 7/20/2016 7/20/2016 | 14:05:00 14:06:00 | -25.2 | | -72.225 | 286.4375 332.3125 | 36.1 | 69.33 68.75 | 7.96 7.86 | | | 8.78 8.93 | | | 22.1812 |
| 7/20/2016 | 14:07:00 | -14.5 -31.75 | | -74.2875 -83.325 | 283.4375 | 31.6 30.8 | | 7.80 | 40.06 40.06 | | 9.03 | | | 22.2787 |
| 7/20/2016 | 14:07:00 | -13.3 | -34.2 | | 323.625 | 21 | | | | | 9.38 | | | 22.393 |
| 7/20/2016 | 14:09:00 | -33.7 | | -87.825 | 293.9375 | 20 | | | | | 9.58 | | | |
| 7/20/2016 | 14:10:00 | -10.2 | | | | 19.8 | | | 40.06 | | 9.71 | | | 22.441 |
| 7/20/2016 | | -46.2 | | -96.375 | 258.375 | 20.1 | | | | | 9.53 | | | 22.52 |
| 7/20/2016 | | -13.7 | | | | 19.6 | | | | | 9.41 | | | 22.863 |
| 7/20/2016 | | -29.9 | | -85.875 | 266.75 | 22.1 | | 7.43 | | | 9.45 | | | |
| 7/20/2016 | | -9.4 | | -68.475 | 342.375 | 24.2 | | 7.58 | | | 9.38 | | | |
| 7/20/2016 | 14:15:00 | -30.25 | -58.75 | | 290.25 | 23.2 | | 7.59 | 40.06 | 12.3 | 9.31 | | 7 812.6 | 23.0 |
| 7/20/2016 | 14:16:00 | -8 | -31.6 | -68.8125 | 332.75 | 24.8 | 77.75 | 7.57 | 40.06 | 11.7 | 9.31 | 1.35 | 5 820.6 | 22.961 |
| 7/20/2016 | 14:17:00 | -23.55 | -45 | -79.6875 | 335.875 | 26.4 | 77.16 | 7.7 | 40.06 | 12.1 | 9.13 | 1.4 | 849.4 | 22.5 |
| 7/20/2016 | 14:18:00 | -6.4 | -29.85 | -69.3 | 359.1875 | 29 | 76.13 | 7.92 | 40.06 | 11.2 | 8.85 | 1.08 | 8 874.2 | 22.7012 |
| 7/20/2016 | 14:19:00 | -27.4 | -48.05 | -88.2375 | 314.625 | 27.9 | 75.91 | 7.94 | 40.06 | 11.7 | 8.83 | 1.3 | 880.8 | 22.993 |
| 7/20/2016 | 14:20:00 | -12.05 | | | 337.875 | | | | | | | | | |
| 7/20/2016 | 14:21:00 | -29.95 | | | 299.875 | | | | | | | | | |
| 7/20/2016 | | -10.25 | | | | 25.6 | | | | | | | | |
| 7/20/2016 | | -17.25 | | | 312.875 | | | | | | | | | |
| 7/20/2016 | | -6.85 | | | | | | | | | | | | |
| 7/20/2016 | | -12.2 | | | 342.75 | | | | | | | | | |
| 7/20/2016 | | -5.6 | | | | | | | | | | | | |
| 7/20/2016 | | -16.15 | | | | | | | | | | | | |
| 7/20/2016 | | -8.65 | | | | | | | | | | | | |
| 7/20/2016 7/20/2016 | | -14.6 | | | | | | | | | | | | |
| 7/20/2016 | | -9.45 | | | | | | | | | | | | |
| 7/20/2016 | | -13.5 -6 | | | 318.6875 333.6875 | | | | | | | | | |
| 7/20/2016 | | -6 -9.1 | | | 333.6875 | | | | | | | | | |
| 7/20/2016 | | -9.1 | | | | | | | | | | | | |
| 7/20/2016 | | -4.5 -14.7 | | | | | | | | | | | | |
| 7/20/2016 | | -9.3 | | | | | | | | | | | | |
| 7/20/2016 | | -9.3 | | | | | | | | | | | | |
| | 14:38:00 | -5.95 | | | | | | | | | | | | |
| 1720,2010 | Average | -13.80 | | | | | | | | | | | | |
| | | | 017760000000000000000000000000000000000 | | | | | | | and the second second second | Demonstration of the second | **** | | 1 |
| July 20, 2016 | | Pressures | A DESCRIPTION OF A DESC | lon e | | Analyzers | | loos | 1000 | | 100 | 10 | Icos | Flows |
| | | ÷ | SDA Inlet | | Baghouse | со | HCI | CO2 | H2O | THC | 02 | Opacity | SO2 | PACFlow |
| Test1 | | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC-F |

| 501 20, 2020 | 110000100 | | | | , mary Lord | | | | | | | | |
|--------------|-------------|-----------|-----------|----------|-------------|----------|----------|----------|----------|----------|----------|----------|-----------|
| | Incinerator | SDA Inlet | SD Outlet | Baghouse | СО | HCI | CO2 | H2O | тнс | 02 | Opacity | SO2 | PACFlow |
| Test1 | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC-FT |
| Max | -4.5 | -23.8 | -54.0 | 360.1 | 38.7 | 78.1 | 8.0 | 40.1 | 16.8 | 12.3 | 1.5 | 889.2 | 23.0 |
| Min | -46.2 | -71.6 | -96.9 | 258.4 | 7.8 | 27.4 | 1.9 | 40.1 | 8.9 | 8.8 | 1.1 | 225.5 | 22.2 |
| Average | -13.8 | -37.6 | -72.0 | 328.9 | 26.8 | 70.4 | 7.6 | 40.1 | 12.0 | 9.2 | 1.3 | 830.1 | 22.6 |
| Variance | 68.29369 | 90.28321 | 79.9499 | 524.0933 | 27.94737 | 72.12033 | 1.054411 | 1.85E-27 | 1.205098 | 0.311435 | 0.007823 | 11828.78 | 0.0729727 |

| TEST 5 | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SDA | Stack |
|--|----------------------|----------------|----------------|----------------------|--------------------|---|----------------------------------|----------------|----------------------|----------------------|----------------|----------------------|----------------|----------------|----------------|-----------------------------|
| | | LPM | | LPM | LPM | | SCFM | | | | | | Degrees C | | | Degrees C |
| Date | Time | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | PV-236 | PV-209 | FT-260C | TE-240 | TE-241 | TE-203 | TE-204 | TE-258 |
| 7/20/2016 | 14:54:00 | 27.03 | 9.715 | 170.3363 | 141.3 | 7.915 | 474.9 | 14.25 | 22504.31 | | 88008 | 1349.5 | 996.6 | 486.8 | 184.5 | 187.6 |
| 7/20/2016 | 14:55:00 | 26.82 | 9.925 | 170.5725 | 140.85 | 7.9225 | 475.35 | 14.25 | | 9505.656 | 88049 | 1346.75 | 997 | 486.6 | 184.5 | 187.6 |
| 7/20/2016 | 14:56:00 | 27.51 | 9.92 | 169.6162 | 140.85 | 6.835 | 410.1 | 14.25 | 22338.41 | | 87814 | 1349.75 | 997 | 485.1 | 184 | 187.6 |
| 7/20/2016 | 14:57:00 | 27.33 | 10.1 | 169.6725 | 140.85 | 7.9225 | 475.35 | 14.25 | 22594.17 | | 87571 | 1349.375 | 997.5 | 484.9 | 183.5 | 186.5 |
| 7/20/2016 | 14:58:00 | 27.375 | 10.04 | 168.9075 | 141.435 | 7.8725 | 472.35 | 14.25 | 22594.17 | 9516.892 | 87962 | 1354.625 | 995.4 | 483.4 | 183 | 186.5 |
| 7/20/2016 | 14:59:00 | 27.27 | 9.965 | 170.3363 | 140.265 | 7.38125 | 442.875 | 14.25 | 22953.63 | 9618.016 | 89952 | 1345.125 | 995.6 | 485.2 | 183 | 186.5 |
| 7/20/2016 | 15:00:00 | 27.3 | 9.625 | 169.4812 | 140.805 | 5.14875 | 308.925 | 14.25 | 22766.99 | 9500.038 | 92819 | 1346.625 | 996.7 | 484.3 | 182.5 | 186.5 |
| 7/20/2016 | 15:01:00 | 27.105 | 9.845 | 169.7175 | 140.85 | 6.21375 | 372.825 | 14.25 | 22684.04 | 9646.106 | 88877 | 1338 | 995.1 | 485.9 | 183 | 186.5 |
| 7/20/2016 | 15:02:00 | 27.18 | 9.845 | 170.19 | 140.85 | 7.91625 | 474.975 | 14.25 | 22504.31 | | 94080 | 1343.375 | 994 | 484.5 | 183 | 186.5 |
| 7/20/2016 | 15:03:00 | 26.985 | 9.985 | 170.145 | 141.39 | 6.375 | 382.5 | 14.25 | 22421.36 | | 87925 | 1339.75 | 993.9 | 485.1 | 183 | 186.5 |
| 7/20/2016 7/20/2016 | 15:04:00 15:05:00 | 27.09 27.21 | 9.965 9.955 | 169.9537 170.7525 | 140.985 141.525 | 7.91625 | 474.975 270.225 | 14.25 14.25 | 22953.63 22684.04 | 9573.072 9584.308 | 94368 88048 | 1346.875 1347.875 | 994.6 994.9 | 483.8 484.7 | 182.5 182.5 | 186.5 |
| 7/20/2016 | 15:06:00 | 26.97 | 9.615 | 169.335 | 141.525 | 6.01375 | 360.825 | 14.25 | 22690.95 | | 93944 | 1354.75 | 994.9 994.3 | 484.7 | 182.5 | 185.4 185.4 |
| 7/20/2016 | 15:07:00 | 27.465 | 10.055 | 169.29 | 141.525 | 7.92125 | 475.275 | 14.25 | 22766.99 | | 88759 | 1343.625 | 995 | 482.0 | 182 | 185.4 |
| 7/20/2016 | 15:08:00 | 27.405 | 9.755 | 169.335 | 141.525 | 7.92123 | 475.2 | 14.25 | 23216.3 | | 93600 | 1346.125 | 994 | 483.6 | 182 | 185.4 |
| 7/20/2016 | 15:09:00 | 27.105 | 10.255 | 171.18 | 140.04 | 7.3525 | 441.15 | 14.25 | 22690.95 | 9505.656 | 88171 | 1342.75 | 992.3 | 485 | 182.5 | 185.4 |
| 7/20/2016 | 15:10:00 | 27.09 | 9.925 | 169.0988 | 139.95 | 6.6425 | 398.55 | 14.25 | 23036.58 | 9522.51 | 94021 | 1342.75 | 992.2 | 484.2 | 182.5 | 180.4 |
| 7/20/2016 | 15:11:00 | 27.225 | 9.92 | | 140.49 | 7.9175 | 475.05 | 14.25 | 22684.04 | 9544.982 | 88938 | 1340.125 | 994 | 484.3 | 182.5 | 185.3 |
| 7/20/2016 | 15:12:00 | 27.615 | 9.875 | 169.7175 | 139.41 | 7.2575 | 435.45 | 14.25 | 23043.49 | 9691.05 | 92306 | 1340.125 | 992.9 | 484.2 | 182.5 | 185.3 |
| 7/20/2016 | 15:12:00 | 27.645 | 9.88 | 169.2 | 139.41 | 7.91875 | 475.125 | 14.25 | 22414.45 | | 87674 | 1347 | 992.9 994.3 | 484.2 | 182.5 | 185.3 |
| 7/20/2016 | 15:14:00 | 27.795 | 9.765 | 169.7625 | 138.825 | 7.64375 | 475.125 | 14.25 | 23126.44 | | 93267 | 1350.875 | 994.3 993.7 | 485.1 | 182.5 | 185.3 |
| 7/20/2016 | 15:15:00 | 27.765 | 9.92 | | 139.275 | 7.89375 | 438.025 | 14.25 | 22684.04 | | 88743 | 1330.873 | 995.1 | 483.1 | 182 | 185.3 |
| 7/20/2016 | 15:16:00 | 27.825 | 9.94 | | 139.273 | 7.91125 | 473.623 | 14.25 | 23126.44 | | 92694 | 1349.123 | 996.3 | 487.4 | 183.5 | 185.3 |
| 7/20/2016 | 15:17:00 | 27.625 | 10.035 | 170.7075 | 137.57 | 7.04375 | 422.625 | 14.25 | 22766.99 | | 88614 | 1348.375 | 992.6 | 488.3 | 183.3 | 185.5 |
| 7/20/2016 | 15:18:00 | 27.885 | 9.62 | | 137.385 | 7.91125 | 474.675 | 14.25 | 22946.71 | 9662.96 | 88553 | 1348.875 | 994 | 487.6 | 184 | 186.4 |
| 7/20/2016 | 15:19:00 | 27.84 | 9.86 | 170.28 | 138.15 | 7.91125 | 474.675 | 14.25 | 22504.31 | | 87394 | 1349.25 | 995.1 | 487.6 | 184.5 | 186.4 |
| 7/20/2016 | 15:20:00 | 27.48 | 9.81 | | 138.915 | 7.91875 | 475.125 | 14.25 | 22684.04 | | 88293 | 1350.125 | 995.8 | 487.6 | 184.5 | 186.4 |
| 7/20/2016 | 15:21:00 | 27.675 | 10.225 | 170.4262 | 139.455 | 7.91625 | 474.975 | 14.25 | | | 87326 | 1356.75 | 993 | 487.6 | 184.5 | 186.4 |
| 7/20/2016 | 15:22:00 | 27.765 | 10.025 | 169.7175 | 138.15 | 7.5825 | 454.95 | 14.25 | 23043.49 | | 89886 | 1356.875 | 995.9 | 487.4 | 184.5 | 186.4 |
| 7/20/2016 | 15:23:00 | 27.585 | 9.93 | | 138.735 | 5.04375 | 302.625 | 14.25 | | | 87865 | 1352 | 992.9 | 488.4 | 185 | 186.4 |
| 7/20/2016 | 15:24:00 | 27.885 | 9.995 | 169.335 | 137.52 | 7.51125 | 450.675 | 14.25 | 23396.02 | | 91131 | 1350.375 | 992.7 | 489.1 | 185 | 187.6 |
| 7/20/2016 | 15:25:00 | 27.645 | 9.995 | | 138.735 | 7.9125 | 474.75 | 14.25 | 22594.17 | | 88671 | 1348.125 | 992.5 | 489.4 | 185.5 | 187.6 |
| 7/20/2016 | 15:26:00 | 27.675 | 9.58 | | 137.34 | 7.91 | 474.6 | 14.25 | | | 88904 | 1349.75 | 994.8 | 488.9 | 185.5 | 188.8 |
| 7/20/2016 | 15:27:00 | 27.735 | 9.805 | | 138.015 | 5.3775 | 322.65 | 14.25 | 22331.5 | | 88425 | 1351.75 | 993.9 | 488.4 | 186 | 187.7 |
| 7/20/2016 | 15:28:00 | 27.72 | 9.87 | 169.4363 | 136.755 | 7.07125 | 424.275 | 14.25 | | | 88970 | 1350.125 | 994.7 | 488.9 | 186 | 187.7 |
| 7/20/2016 | 15:29:00 | 27.735 | 10.085 | 170.0437 | 138.69 | 7.91125 | 474.675 | 14.25 | 22331.5 | | 86999 | 1352.625 | 994 | 487.8 | 186 | 187.7 |
| 7/20/2016 | 15:30:00 | | 9.995 | | 136.485 | 7.9075 | 474.45 | 14.25 | | | 89812 | 1349.875 | 994.2 | 489.1 | 185.5 | 188.8 |
| 7/20/2016 | 15:31:00 | | 10.24 | 169.7625 | 137.61 | 7.90875 | 474.525 | 14.25 | | | 87909 | 1353.75 | 995.1 | 489.1 | 186 | 187.8 |
| 7/20/2016 | 15:32:00 | | 9.735 | 171 | 135.765 | 7.91 | 474.6 | 14.25 | | | 89864 | 1346.25 | 995.8 | 490.8 | 186.5 | 187.8 |
| 7/20/2016 | 15:33:00 | | 9.92 | 170.1 | 136.89 | 7.9175 | 475.05 | 14.25 | | | 87605 | 1349.375 | 994.9 | 490.4 | 187 | 187.8 |
| 7/20/2016 | 15:34:00 | | 9.965 | | 135.135 | 7.915 | 474.9 | 14.25 | | | 88127 | 1350.5 | 996.1 | 490.7 | 187.5 | 187.8 |
| 7/20/2016 | 15:35:00 | | 9.825 | 170.145 | 135.765 | 7.9175 | 475.05 | 14.25 | | | 87711 | 1355 | 994.3 | 490.3 | 187.5 | 187.8 |
| 7/20/2016 | 15:36:00 | | 9.82 | | 134.685 | 7.91375 | 474.825 | 14.25 | | | 87732 | | 994.2 | 490.9 | 188 | 187.8 |
| 7/20/2016 | 15:37:00 | | 9.885 | 170.9437 | 135.765 | 7.0475 | 422.85 | 14.25 | | | 86082 | 1357.25 | 996.5 | 490.3 | 188 | 187.8 |
| | | | 9.9 | | 134.64 | 7.61125 | 456.675 | 14.25 | | | 88489 | 1356.125 | 997 | 491.6 | 188 | 187.8 |
| 7/20/2016 | | | 10.05 | 171.2813 | 135.225 | 6.38375 | 383.025 | 14.25 | | 9612.398 | | 1357.5 | 997.5 | 492.4 | 189 | 187.8 |
| 7/20/2016 | | | | 171.5625 | | 7.91625 | 474.975 | 14.25 | | 9674.196 | | 1353.5 | 999 | | 189.5 | 189 |
| 7/20/2016 | | | | | | 7.9175 | 475.05 | 14.25 | | 9556.218 | | 1359 | 996 | | | 189.1 |
| | 15:42:00 | | | | | | 474.975 | 14.25 | | 9556.218 | | 1356.375 | 997.1 | | | 190.2 |
| 7/20/2016 | | | | | | | 475.125 | 14.25 | | 9556.218 | | | 998.8 | | 190.5 | 189 |
| 7/20/2016 | | | | | | 7.915 | 474.9 | 14.25 | | 9539.364 | | 1358.625 | 998.5 | 494.7 | | 189.9 |
| 7/20/2016 | 15:45:00 | 27.915 | 9.985 | 170.6175 | | | 474.9 | 14.25 | 22331.5 | 9539.364 | 86568 | 1361.375 | 997.6 | 494.9 | 190.5 | 189.9 |
| 7/20/2016 | 15:46:00 | | | 173.0363 | 135.18 | 7.9175 | 475.05 | 14.25 | | 9640.488 | 88530 | 1361.125 | 999.1 | 496.4 | 190.5 | |
| 7/20/2016 | 15:47:00 | 27.72 | 9.98 | 170.7075 | 136.035 | 7.91625 | 474.975 | 14.25 | 22511.22 | 9640.488 | 87378 | 1360 | 998.4 | 497.2 | 191 | 189.9 |
| 7/20/2016 | 15:48:00 | 27.57 | 10.21 | 171.18 | 135.945 | 7.9175 | 475.05 | 14.25 | 22684.04 | 9629.252 | 88479 | 1355.625 | 999.6 | 498.4 | 191.5 | |
| 7/20/2016 | 15:49:00 | 27.855 | 10.025 | 171.6075 | 136.665 | 7.92125 | 475.275 | 14.25 | 22331.5 | 9528.128 | 86979 | 1361.125 | 999.2 | 497.4 | 191 | 190.7 |
| 7/20/2016 | 15:50:00 | 27.9 | 10.105 | 170.8088 | 135.18 | 7.925 | 475.5 | 14.25 | 22511.22 | 9494.42 | 87214 | 1360.5 | 998.4 | 497.9 | 191 | |
| 7/20/2016 | 15:51:00 | 27.705 | 9.99 | 170.3363 | 135.18 | | 475.35 | 14.25 | 22241.64 | 9595.544 | 85298 | 1365.125 | 1000.4 | 496.7 | 191 | 190.7 |
| 7/20/2016 | 15:52:00 | 27.9 | 9.445 | 171.7538 | 134.055 | | 474.9 | 14.25 | 22511.22 | 9595.544 | 87221 | 1360.875 | 999.5 | 497.2 | 191 | 190.7 |
| 7/20/2016 | 15:53:00 | 27.615 | 9.745 | 170.3363 | 134.595 | 7.915 | 474.9 | 14.25 | 22151.77 | 9595.544 | 85041 | 1362.375 | 999.3 | 496 | 191 | 190.7 |
| 7/20/2016 | 15:54:00 | | | | 133.38 | | 474.975 | 14.25 | | 9595.544 | | 1353.125 | | 497.4 | 191.5 | 190.7 |
| | | | | | | | | | | | | | | | | |
| | Average | 27.57 | 9.91 | 170.36 | 137.90 | 7.48 | 449.05 | 14.25 | 22657.07 | 9574.55 | 88839.07 | 1351.70 | 995.74 | 489.27 | 185.96 | 187.60 |
| July 20, 2016 | | Waste Flo | WS | <u></u> | | 05.000770000000000000000000000000000000 | Second Contraction of the second | | Air Flows | | | Temperati | ires | | · . | NEWSCOMPOSICION CONCERNMENT |
| | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SprayDryer | Stack |
| Test1 | | FT-229 | FT-219C | FT-223 | PV-207 | FT-313B | FT-313 | PV-211 | PV-236 | PV-209c | FT-260c | TE-240 | TE-241 | TE-203 | TE-204 | TE-258 |
| Max | | 28.0 | 10.3 | 173.0 | 141.5 | 7.9 | 475.5 | 14.3 | 23396.0 | 9691.1 | 94368.0 | 1365.1 | 1000.4 | 498.4 | 191.5 | 190.7 |
| Min | | 26.8 | 9.4 | 168.9 | 133.4 | 4.5 | 270.2 | 14.3 | 22151.8 | 9415.8 | | 1338.0 | 992.2 | 482.6 | 182.0 | 185.3 |
| Average | | 27.6 | 9.9 | 170.4 | 137.9 | 7.5 | | 14.3 | 22657.1 | 9574.5 | 88839.1 | 1351.7 | 995.7 | 489.3 | 186.0 | 187.6 |
| Variance | | 0.083696 | 0.025484 | 0.702875 | | | | 0 | 72991.366 | 3932.512 | 4873925.1 | 37.57561 | 4.685055 | 20.0413 | 10.44413 | 2.972831 |
| Beating a surrow of the second se | | ¢ | ****** | | | ***** | L | · | | | | · | · | | · | |

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| TEST 5 | | Incinerato | SDA Inlet | BH Inlet | BH dP | со | нсі | CO2 | H2O | тнс | 02 | Opacity | 502 | PAC |
|---------------------------------------|----------------------|-----------------|-----------|----------------|---------------------|--------------|----------------|--------------|--|-----------|--------------|---------|----------|-----------|
| 12010 | | mmH2O | mmH2O | mmH2O | mmH2O | PPM | PPM | % | % | PPM | % | % | PPM | Lbs/h |
| Date | Time | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205COF | AT-213A | AT-213B | AT-213C | AT-259COF | AT-261 | AT-263 | AT-264 | SC-PAC-FT |
| 7/20/2016 | 14:54:00 | -7.7 | | -60.825 | 342.3125 | 27.4 | 66.41 | 7.76 | 40.06 | 12.3 | 9.13 | 1.37 | 857.4 | 22.23 |
| 7/20/2016 | 14:55:00 | -10.4 | | | 322 | 27.6 | 67.41 | 7.83 | | | 9.13 | | | 22.44125 |
| 7/20/2016 | 14:56:00 | -7.7 | | | 288.75 | 27.8 | 65.82 | 7.75 | | | 9.18 | | | 22.7825 |
| 7/20/2016 | 14:57:00 | -8.6 | | -67.8 | 351.875 | 27.7 | 66.67 | 7.89 | | | 9.11 | | | |
| 7/20/2016 7/20/2016 | 14:58:00 14:59:00 | -8.4 11.75- | | -60.9 -68.7 | 274.25 332.3125 | 27.9 | 66.84 | 7.89 | | | 9.03 | | | |
| 7/20/2016 | 15:00:00 | -23.15 | | | 262.375 | 27.6 25.9 | 65.29 64.2 | 7.9 7.85 | | | 8.86 8.89 | | | |
| 7/20/2016 | 15:01:00 | -12.7 | | | 332.125 | 22.3 | 64.37 | 7.03 | | | 9.08 | | | |
| 7/20/2016 | 15:02:00 | -26.65 | | | | 21.8 | 67.26 | 7.66 | | | 9.14 | | | |
| 7/20/2016 | 15:03:00 | -9.85 | | -70.125 | | 23.6 | 69.19 | 7.69 | | | 9.11 | | | |
| 7/20/2016 | 15:04:00 | -31.95 | -60.6 | -76.125 | 263.5 | 24.3 | 69.37 | 7.69 | 40.06 | 11.7 | 9.21 | . 1.4 | 849.2 | 22.24625 |
| 7/20/2016 | 15:05:00 | -6.6 | -31.1 | -64.425 | 351.6875 | 24.9 | 69.43 | 7.77 | 40.06 | 11.4 | 9.23 | 1.18 | 858.2 | 22.76625 |
| 7/20/2016 | 15:06:00 | -30.7 | -60.05 | -77.175 | 254.875 | 25.6 | 70.45 | 7.86 | 40.06 | 11.8 | 8.99 | 1.25 | 868.1 | 22.7175 |
| 7/20/2016 | 15:07:00 | -12.05 | | | | 27.4 | 68.12 | 7.9 | | 11 | 8.88 | | | |
| 7/20/2016 | | -30.75 | | | | 26.4 | 67.14 | 7.86 | | | | | | |
| 7/20/2016 | | -10.05 | | | 336.75 | 24.7 | 67.23 | 7.79 | | | | | | |
| 7/20/2016 | | -29.85 | | | | 25.2 | 67.82 | 7.73 | | | | | | |
| 7/20/2016 7/20/2016 | | -9.65 -31.15 | | | 327.8125 306.5 | 23.6 23.7 | 69.17 68.52 | 7.67 7.68 | | | | | | |
| 7/20/2016 | | -51.15 | | | | 23.7 | | 7.83 | | | | | | |
| 7/20/2016 | | -32.05 | | | | 24.8 | 70.45 | 7.93 | | | | | | |
| 7/20/2016 | | -11 | | | 336.25 | 27.1 | | 7.93 | | | | | | |
| 7/20/2016 | | -29.1 | | | 271.5 | 25.7 | | 7.9 | | | | | | |
| 7/20/2016 | | -8.9 | | | | 25.9 | 68.65 | 7.9 | | | | | | |
| 7/20/2016 | 15:18:00 | -14.65 | -37.3 | -78.225 | 315.5625 | 25 | 70.39 | 7.85 | 40.06 | 11.2 | 9.02 | 1.37 | 868.9 | 23.01 |
| 7/20/2016 | 15:19:00 | -8.5 | -30.45 | -62.7375 | 332.5625 | 23.8 | 71.76 | 7.83 | 40.06 | 10.9 | Ş | 1.42 | 870.4 | 22.5875 |
| 7/20/2016 | | -11.3 | | | | 24.2 | 70.78 | 7.8 | | | | | | |
| 7/20/2016 | | -6.1 | | | 358 | 27 | | 7.99 | | | | | | |
| 7/20/2016 | | -17.7 | | | | 28.6 | | 8.01 | | | | | | |
| 7/20/2016 | | -9.35 | | | | 29.7 | | 8 | | | | | | |
| 7/20/2016 7/20/2016 | | -21.15 -8.45 | | | | 26.8 26 | | 7.9 7.87 | | | | | | |
| 7/20/2016 | | -13.1 | | | | 25 | | 7.87 | | | | | | |
| 7/20/2016 | | -8.5 | | | | 25.5 | | 7.79 | | | | | | |
| 7/20/2016 | | -11.1 | | | 345.625 | 26.5 | | 7.77 | | | | | | |
| 7/20/2016 | | -2.95 | | | | | | 7.92 | | | | | | |
| 7/20/2016 | 15:30:00 | -14.9 | -39.4 | -80.025 | 322.875 | 27 | 70.53 | 7.91 | 40.06 | | | 1.37 | 7 892.1 | 22.2625 |
| 7/20/2016 | 15:31:00 | -7 | | -60.2625 | 338.4375 | 27.9 | 69.03 | 7.93 | 40.06 | 11 | 8.8 | 3 1.25 | 5 898.4 | 22.70125 |
| 7/20/2016 | | -14.25 | | -78.15 | 325.6875 | 26.3 | 67.99 | 7.96 | 40.06 | 11.3 | 8.88 | 3 1.31 | L 895.9 | |
| 7/20/2016 | | -7.25 | | | | 26.8 | | 7.96 | | | | | | |
| 7/20/2016 | | -11.9 | | | | 26.6 | | | | | | | | |
| 7/20/2016 | | -4.1 | | | 333.5 | 25.2 | | | | | | | | |
| 7/20/2016 | | -6.75 | | | | 26.5 | | | | | | | | |
| 7/20/2016 7/20/2016 | 15:37:00 15:38:00 | -2 -11.55 | | | 360.375 328.375 | 26.3 28 | | | | | | | | |
| · · · · · · · · · · · · · · · · · · · | 15:38:00 | -11.55 -8.55 | | | 342.6875 | 28 | | | | | | | | |
| 7/20/2016 | | -11.5 | | | | | | | | | | | | |
| 7/20/2016 | | -5.55 | | | 343.0625 | | | | | | | | | |
| 7/20/2016 | | -9 | | | | | | | | | | | | |
| 7/20/2016 | | -6.1 | | | | | | | | | | | | |
| 7/20/2016 | | -5.8 | -28.55 | -44.175 | 350.125 | 28.7 | 73.05 | 7.94 | 40.06 | 10.9 | 8.96 | 5 1.15 | 5 893.1 | |
| 7/20/2016 | | -1.05 | | | 361.5625 | | | | | | | | | |
| 7/20/2016 | | -8.25 | | | | | | | | | | | | |
| 7/20/2016 | | -6.65 | | | | | | | | | | | | |
| 7/20/2016 | | -9.9 | | | | | | | | | | | | |
| 7/20/2016 | | -4 | | | 346.4375 | | | | | | | | | |
| 7/20/2016 | 15:50:00 15:51:00 | -7.05 -3.5 | | | 329.375 339.8125 | | | | | | | | | |
| 7/20/2016 | | -3.5 | | | | | | | | | | | | |
| | 15:53:00 | -2.95 | | | | | | | | | | | | |
| | 15:54:00 | -9.6 | | | | | | | | | | | | |
| ,, | | | | | | | | 5.2 | | 2010 | 5.5 | | | |
| | Average | -11.83 | -36.53 | -66.16 | 325.55 | 26.57 | 70.13 | 7.92 | 40.06 | 11.23 | 8.92 | 2 1.29 | 9 885.03 | 22.58 |
| bib 20. 2010 | | Drocourte | | | | Anaburar | | | 11-14-14-14-14-14-14-14-14-14-14-14-14-1 | | | | | Flows |
| July 20, 2016 | | Pressures | | | - | Analyzers | - | | ingtermetationale distinutioner or | | - | | | Flows |

| July 20, 2016 | Pressures | Pressures | | | Analyzers | Analyzers | | | | | | | | | |
|---------------|-------------|-----------|-----------|----------|-----------|-----------|----------|----------|----------|----------|----------|----------|-----------|--|--|
| | Incinerator | SDA Inlet | SD Outlet | Baghouse | CO | НСІ | CO2 | H2O | THC | 02 | Opacity | SO2 | PACFlow | | |
| Test1 | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC-FT | | |
| Max | -1.1 | -23.1 | -44.2 | 361.6 | 30.3 | 76.2 | 8.2 | 40.1 | 12.3 | 9.3 | 1.4 | 937.0 | 23.1 | | |
| Min | -32.1 | -61.7 | -87.7 | 254.9 | 21.8 | 64.2 | 7.7 | 40.1 | 10.3 | 8.5 | 1.1 | 842.7 | 22.2 | | |
| Average | -11.8 | -36.5 | -66.2 | 325.6 | 26.6 | 70.1 | 7.9 | 40.1 | 11.2 | 8.9 | 1.3 | 885.0 | 22.6 | | |
| Variance | 68.92139 | 104.4443 | 100.4532 | 826.3675 | 3.395628 | 8.002532 | 0.018875 | 1.85E-27 | 0.170448 | 0.038743 | 0.008107 | 547.7903 | 0.0827055 | | |

| TEST 6 | | | | | Alkaline | | TDU Flow | Leachate | Primary | Secondary | | | Secondary | | | Stack |
|---------------------------------------|---|-----------|----------|--|----------|--|----------------|---|-----------|-----------|---|--------------------------------------|--------------------------|--|--|----------|
| ~ | | LPM | LPM | (menone and the second se | LPM | LPM | SCFM | LPM | m3/h | | Management and an | contractor of the contractor and the | ************************ | Contractors and an | Construction and the Construction of the | Degree |
| THE OWNER AND ADDRESS OF | menonenanter and the second | | FT-219C | and the second second second second | PV-207 | ************************************** | FT-313 | PV-211 | PV-236 | | | TE-240 | TE-241 | | and the second sec | TE-258 |
| 7/20/2016 | 16:05:00 | 27.645 | 9.925 | | 133.155 | 7.91 | 474.6 | 14.25 | 22594.17 | 9567.454 | 92298 | 1360.125 | 1000.1 | | 190.5 | 19 |
| 7/20/2016 | 16:06:00 | 27.81 | 9.98 | | 133.2 | | 475.125 | 14.25 | 22338.41 | 9455.094 | 87274 | 1363.875 | 999.3 | | 190 | 19 19 |
| 7/20/2016 | 16:07:00 | 27.525 | 9.955 | | 133.155 | 7.91 | 474.6 | 14.25 | 22690.95 | 9556.218 | 92737 | 1365.875 1364.875 | 1001.8 | | 189.5 | |
| 7/20/2016 | 16:08:00 | 27.675 | | 170.5162 | 134.37 | 7.91375 | 474.825 | 14.25 | 22158.69 | 9455.094 | 86595 | | 999.7 | | 189.5 | 1 |
| 7/20/2016 | 16:09:00 | 27.465 | | 170.3363 | 134.46 | 7.92125 | 475.275 | 14.25 | 22953.63 | 9584.308 | 93852 | 1368.125 | 999.6 | | 188.5 | 1 |
| 7/20/2016 | 16:10:00 | 27.765 | 9.98 | | 134.595 | 7.9225 | 475.35 | 14.25 | 22773.9 | 9584.308 | 88193 | 1367.25 | 999.7 | | 189 | 1 |
| 7/20/2016 | 16:11:00 | 28.14 | 10.13 | | 133.965 | 7.92625 | 475.575 | 14.25 | 22953.63 | 9595.544 | 93164 | 1366 | 999.5 | | 188.5 | - |
| 7/20/2016 | 16:12:00 | 27.705 | 9.88 | 170.1 | 134.64 | 7.9275 | 475.65 | 14.25 | 22421.36 | 9595.544 | 87247 | 1360.5 | 1001.3 | | 189 | : |
| 7/20/2016 | 16:13:00 | 27.495 | 10.13 | | 134.1 | 7.2625 | 435.75 | 14.25 | 22953.63 | 9719.14 | 93842 | 1361.375 | 1000.3 | | 188 | : |
| 7/20/2016 | 16:14:00 | 27.795 | 9.665 | | 132.885 | 7.91125 | 474.675 | 14.25 | 22421.36 | 9612.398 | 86809 | 1363.25 | 1001.7 | | 188 | : |
| 7/20/2016 | 16:15:00 | 27.705 | 9.87 | 169.29 | 132.12 | 7.9125 | 474.75 | 14.25 | 22773.9 | 9623.634 | 89126 | 1364.75 | 1001.7 | | 187.5 | |
| 7/20/2016 | 16:16:00 | 28.005 | | 170.0437 | 132.66 | 5.495 | 329.7 | 14.25 | 22241.64 | 9500.038 | 86705 | 1367.375 | 1000 | | 188 | |
| 7/20/2016 | 16:17:00 | 27.585 | 9.73 | | 132.84 | 7.915 | 474.9 | 14.25 | 22863.76 | 9612.398 | 92019 | 1366.125 | 1001.6 | 486.2 | 187.5 | |
| 7/20/2016 | 16:18:00 | 27.945 | 9.865 | 169.8075 | 133.38 | 7.91875 | 475.125 | 14.25 | 22601.09 | 9612.398 | 87772 | 1362.5 | 1000.4 | 486.8 | 188 | |
| 7/20/2016 | 16:19:00 | 27.78 | 9.55 | 170.7525 | 132.795 | 7.91875 | 475.125 | 14.25 | 23126.44 | 9584.308 | 92608 | 1361.875 | 999.9 | 487.2 | 187.5 | |
| 7/20/2016 | 16:20:00 | 27.735 | 10.14 | 171 | 134.46 | 7.91375 | 474.825 | 14.25 | 22331.5 | 9584.308 | 88081 | 1361.625 | 1000.7 | 488.6 | 188.5 | |
| 7/20/2016 | 16:21:00 | 27.45 | 9.875 | 170.5725 | 133.83 | 7.92125 | 475.275 | 14.25 | 22863.76 | 9691.05 | 88362 | 1362.125 | 1002 | 488.4 | 188 | |
| 7/20/2016 | 16:22:00 | 27.915 | 10.17 | 169.29 | 134.55 | 7.92375 | 475.425 | 14.25 | 22248.55 | 9466.33 | 87153 | 1364.375 | 1001.5 | 487.5 | 188 | |
| 7/20/2016 | 16:23:00 | 27.675 | 9.895 | 170.145 | 132.795 | 7.91375 | 474.825 | 14.25 | 22773.9 | 9629.252 | 87608 | 1364.375 | 1001.9 | | 187.5 | |
| 7/20/2016 | 16:24:00 | 27.525 | 10.035 | | 133.92 | | 474.975 | 14.25 | 22338.41 | 9528.128 | 86769 | 1367.875 | 1001.6 | | 187.5 | |
| 7/20/2016 | 16:25:00 | 27.765 | | 169.9537 | 133.38 | | 475.275 | 14.25 | 23043.49 | 9747.23 | 88444 | 1363.625 | 1002.2 | | 187.5 | |
| 7/20/2016 | 16:26:00 | 27.51 | | 168.6712 | 133.425 | 7.92 | 475.2 | | 22594.17 | | 88166 | 1362.75 | 1002.2 | | 188 | |
| 7/20/2016 | 16:27:00 | 27.69 | 9.86 | | 132.885 | 7.915 | 474.9 | 14.25 | 23126.44 | 9668.578 | 89424 | 1360.25 | 997.8 | | 188 | |
| 7/20/2016 | 16:28:00 | 27.885 | 10.05 | | 133.47 | 7.9225 | 475.35 | 14.25 | 22338.41 | | 87607 | 1357.375 | 1002 | | 188.5 | |
| 7/20/2016 | 16:29:00 | 27.885 | 9.535 | | 132.345 | 7.9225 | 475.35 | 14.25 | 22953.63 | 9691.05 | 8784 | 1358.875 | 1002 | | 188 | |
| 7/20/2016 | 16:29:00 | 27.615 | | 169.0087 | 132.545 | 7.9223 | 475.55 | | 22595.05 | 9578.69 | | | 1000.5 | | | |
| | | | | | | | | | 22594.17 | 9685.432 | 86260 | 1362.25 | | | 188.5 | |
| 7/20/2016 | 16:31:00 | 27.6 | | 169.6162 | 132.165 | 7.91625 | 474.975 | 14.25 | | | 87662 | 1363 | 1001.2 | | 188 | |
| 7/20/2016 | 16:32:00 | 27.465 | | 170.6175 | 133.245 | 7.9125 | 474.75 | 14.25 | 22421.36 | 9578.69 | 86622 | 1371.5 | 1002.3 | | 188 | |
| 7/20/2016 | 16:33:00 | 27.93 | | 169.9537 | 132.705 | 7.915 | 474.9 | | 22863.76 | | 89029 | 1366.5 | 999 | | 188 | |
| 7/20/2016 | | 27.81 | | 170.5162 | 133.83 | 7.9225 | 475.35 | | 22511.22 | | 87624 | 1359.875 | 1002.5 | | 188 | |
| 7/20/2016 | | 27.84 | | 170.0437 | 133.065 | 7.9225 | 475.35 | | 22863.76 | | 88272 | 1355.75 | 999.9 | | 188 | |
| 7/20/2016 | 16:36:00 | 27.555 | 10.015 | 170.7525 | 134.235 | 7.91625 | 474.975 | 14.25 | 22511.22 | 9606.78 | 87306 | 1359.25 | 1003 | 489.1 | 188.5 | |
| 7/20/2016 | 16:37:00 | 27.78 | 10.02 | 170.8088 | 133.56 | 7.9275 | 475.65 | 14.25 | 22421.36 | 9713.522 | 88173 | 1359.25 | 1000.1 | . 488.9 | 188.5 | |
| 7/20/2016 | 16:38:00 | 27.795 | 9.99 | 169.4812 | 133.56 | 7.92875 | 475.725 | 14.25 | 22421.36 | 9483.184 | 86497 | 1366.875 | 1002.9 | 487.9 | 188.5 | |
| 7/20/2016 | 16:39:00 | 27.96 | 9.875 | 170.6175 | 132.255 | 7.92125 | 475.275 | 14.25 | 22690.95 | 9573.072 | 87176 | 1367.25 | 1001.8 | 487.9 | 188.5 | |
| 7/20/2016 | 16:40:00 | 27.945 | 9.85 | 170.6175 | 133.38 | 7.59625 | 455.775 | 14.25 | 22248.55 | 9573.072 | 85916 | 1377 | 1001.4 | 486.2 | 188 | |
| 7/20/2016 | 16:41:00 | 27.75 | 9.935 | 170.4713 | 132.48 | 7.91375 | 474.825 | 14.25 | 22684.04 | 9685.432 | 87664 | 1369 | 1001 | 487.7 | 188 | |
| 7/20/2016 | 16:42:00 | 27.555 | 9.875 | 169.1437 | 133.965 | 7.925 | 475.5 | 14.25 | 22421.36 | 9578.69 | 87063 | 1371 | 1000.6 | 6 487.7 | 188.5 | |
| 7/20/2016 | 16:43:00 | 27.72 | 9.805 | 169.8075 | 139.59 | 7.92 | 475.2 | | 22863.76 | | 88192 | 1362.375 | 1002.6 | 6 488.4 | 188 | |
| 7/20/2016 | | 27.945 | | 169.9537 | 140.895 | 7.92375 | 475.425 | | 22511.22 | | 87664 | 1366.375 | 999.8 | | 187 | |
| 7/20/2016 | 16:45:00 | 27.675 | | 170.5725 | 140.355 | | 475.125 | | 22684.04 | | 87965 | 1362.125 | 999.6 | | 186 | |
| 7/20/2016 | | 27.69 | 9.945 | | 141.57 | 7.825 | 469.5 | | 22511.22 | | 87252 | | 999.3 | | 185 | |
| 7/20/2016 | 16:47:00 | 27.63 | 9.95 | | 140.895 | | 475.65 | | 22511.22 | | 87494 | 1367.025 | 1000.7 | | 184.5 | |
| 7/20/2016 | 16:48:00 | 27.05 | 10.085 | | 140.855 | | 475.8 | | 22331.22 | | 85661 | 1368.25 | 999.5 | | 184.5 | |
| | | | | | | | | | | | | | | | | |
| 7/20/2016 | | 27.78 | 10 | | 141.525 | | 475.05 | | | | 88928 | | 1001.4 | | 184 | |
| 7/20/2016 | | 27.57 | | | 140.715 | | | | | | | 1363.625 | | | 184 | |
| 7/20/2016 | | 27.87 | | 170.7075 | 139.95 | | | | | 9696.668 | | 1359.625 | | | | |
| 7/20/2016 | | 28.11 | | | 140.535 | | | | | | | | | | 184 | |
| 7/20/2016 | | 27.78 | | 169.9988 | 139.725 | | | | | 9589.926 | | | | | | |
| 7/20/2016 | | 28.17 | | 169.5263 | 139.68 | | | | | 9589.926 | | 1363.625 | | | | |
| 7/20/2016 | | 27.72 | | 169.9088 | 140.31 | | | | | 9567.454 | | 1358.875 | | | | |
| 7/20/2016 | | 27.765 | | 170.6175 | 140.895 | 7.92 | 475.2 | 14.25 | 22338.41 | 9567.454 | 86420 | 1363.625 | 1003 | 496.2 | 184.5 | |
| 7/20/2016 | 16:57:00 | 27.66 | 10.065 | 169,9088 | 140.22 | 7.9225 | 475.35 | 14.25 | 22511.22 | 9595.544 | 87982 | 1356.25 | 1002.9 | 498.5 | 184.5 | |
| 7/20/2016 | 16:58:00 | 27.825 | 9.85 | 169.38 | 141.885 | 7.9225 | 475.35 | 14.25 | 22863.76 | 9595.544 | 92719 | 1358 | 1002.3 | 498.5 | 184.5 | |
| 7/20/2016 | 16:59:00 | 28.11 | 10.05 | 171.045 | 141.165 | 7.9225 | 475.35 | 14.25 | 22766.99 | 9634.87 | 88210 | 1352.375 | 1002.3 | 499.3 | 185 | |
| 7/20/2016 | | 27.72 | | 169.9088 | 141.66 | | | | | 9629.252 | | 1358.125 | | | | |
| 7/20/2016 | | 27.78 | | 170.6625 | 141.75 | | | | | 9528.128 | | 1355.375 | | | | |
| 7/20/2016 | | 27.9 | | 169.0988 | 140.49 | | | | | | | | | | | |
| 7/20/2016 | | 27.87 | | 169.0988 | 140.445 | | | | | | | 1358.125 | | | | |
| 7/20/2016 | | 27.57 | | 169.5263 | 139.725 | | | | | | | | | | | |
| 7/20/2016 | | 27.69 | | | 133.723 | | | | | | | 1356.625 | | | | |
| ., 20, 2010 | 27.00.00 | 27.03 | 10.023 | 1, 1.03 | 140.4 | 1.52 | -1 <i>3.</i> 2 | 14.23 | 5.5113.3 | 0.000 | 00441 | 1990.023 | 1003.3 | 30.3 | 104.3 | |
| | Average | 27.76 | 9.92 | 170.00 | 136.16 | 7.83 | 469.53 | 14.25 | 22621.71 | 9599.14 | 88561.13 | 1362.99 | 1001.11 | 490.45 | 186.97 | ' 1 |
| July 20, 2016 | ; 1 | Waste Flo | WS | | | | | | Air Flows | | | Temperatu | ires | | | ******* |
| ,, | | Rich | Emulsion | Lean | Alkaline | TDU Flow | TDU Flow | Leachate | Primary | Secondary | Stack | Primary | Secondary | Quench | SprayDrye | distar |
| Test1 | 573-578-1570-1570-1570-1570-1570-1570-1570-1570 | FT-229 | FT-219C | FT-223 | PV-207 | | | PV-211 | | | | <u> </u> | | | | |
| NOTION AND INCOMENDATION OF THE OWNER | **** | | A | | | FT-313B | FT-313 | Contraction and the Contraction of the Contraction | PV-236 | PV-209c | FT-260c | TE-240 | TE-241 | TE-203 | TE-204 | TE-2 |
| Max | | 28.2 | 10.2 | 171.1 | 142.2 | ÷ | | + | -f | | | 1377.0 | | | | |
| Min | | 27.5 | | | 132.1 | 5.5 | <u> </u> | | | 9455.1 | 85661.0 | 1352.4 | | | | |
| | | 27.8 | 9.9 | 170.0 | 136.2 | 7.8 | 469.5 | 14.3 | 22621.7 | 9599.1 | 88561.1 | 1363.0 | 1001.3 | 490.5 | 187.0 | 1 |
| Average Variance | | 0.030453 | | | 13.3311 | 0.184979 | 665.9237 | C | 60565.901 | 4406.079 | 4968209.9 | 19.4412 | 1.634699 | 24.22252 | 3.63224 | 1.7 |

| TEST 6 | | Incinerator | | | BH dP | | HCI | CO2 | H2O | тнс | 02 | Opacity | 502 | PAC |
|---|----------------------------|--|------------------|--|---------------------|-----------------|----------------|--------------|----------------|--------------|--------------|---------|----------|----------------------|
| | | mmH2O | mmH2O | THE OWNER AND ADDRESS OF ADDRESS | mmH2O | PPM | PPM | % | % | PPM | % | % | PPM | Lbs/h |
| Contractive Contraction of the Contraction of the | Time | CONTRACTOR OF CONT | PT-249 | reason and a second sec | PDT-622 | AT-205COR | | AT-213B | AT-213C | AT-259COF | | AT-263 | AT-264 | SC-PAC-FT |
| 7/20/2016 | 16:05:00 | -28 | -57.3 | -65.925 | 258.1875 | 25.4 | 74.75 | 7.99 | 40.06 | 11.4 | 8.79 | | | 22.88 |
| 7/20/2016 7/20/2016 | 16:06:00 16:07:00 | -5.2 | -29.9 | -52.4625 | 326.3125 263.625 | 25.2 | 76.2 | 7.96 | | 10.7 | 8.72 | | | 22.88 22.6525 |
| 7/20/2016 | 16:07:00 | -28.8 -5.65 | -59.55 -30.65 | -65.85 -47.5875 | 352.9375 | 26.6 28.6 | 74.88 74.46 | 7.91 8.09 | 40.06 40.06 | 11.7 10.8 | 8.82 8.64 | | | 22.24625 |
| 7/20/2016 | 16:09:00 | -28.85 | -59.6 | -47.3873 | 256.6875 | 28.0 | 74.40 | 8.12 | | 10.8 | 8.55 | | | 22.4575 |
| 7/20/2016 | 16:10:00 | -5.7 | -28.25 | -63.9 | 335.25 | 31.3 | 71.63 | 8.15 | 40.06 | 10.6 | | | | 22.21375 |
| 7/20/2016 | 16:11:00 | -27.3 | -55.2 | -74.475 | 262.875 | 29.9 | 69.92 | 8.11 | | 11.3 | 8.51 | | | 22.76625 |
| 7/20/2016 | 16:12:00 | -6.05 | -29.65 | -50.325 | 337.875 | 27.2 | 70.67 | 8.06 | | 10.6 | | | | 22.75 |
| 7/20/2016 | 16:13:00 | -24.2 | -45.05 | -75.075 | 290.5625 | 26.4 | 71.64 | 8.05 | | | | | | 22.945 |
| 7/20/2016 | 16:14:00 | -4.8 | -27.25 | -51 | 329.4375 | 25.8 | 72.87 | 8.02 | | | 8.65 | | | 22.3925 |
| 7/20/2016 | 16:15:00 | -8.85 | -32.8 | -66.975 | 337.6875 | 25.5 | 71.92 | 7.97 | | | | | | 22.8475 |
| 7/20/2016 | 16:16:00 | -2.9 | -26.9 | -45 | 356.625 | 25.8 | 73.24 | 8.12 | 40.06 | 10.8 | 8.69 | 1.12 | 908.8 | 22.24625 |
| 7/20/2016 | 16:17:00 | -18.85 | -43.8 | -81.75 | 311 | 25.7 | 74.33 | 8.2 | 40.06 | 11.4 | 8.55 | 1.3 | 918.2 | 22.2625 |
| 7/20/2016 | 16:18:00 | -7.7 | -33.1 | -60.9 | 336.25 | 26.7 | 73.86 | 8.21 | 40.06 | 10.7 | 8.48 | 1.21 | . 924 | 22.89625 |
| 7/20/2016 | 16:19:00 | -23.6 | -52.2 | -80.0625 | 288.125 | 26.5 | 72.99 | 8.06 | 40.06 | 11.4 | 8.61 | 1.33 | 912.8 | 22.27875 |
| 7/20/2016 | 16:20:00 | -6.2 | -30.55 | -58.0875 | 341.625 | 26.4 | 74.85 | 7.99 | | | | | | 22.86375 |
| 7/20/2016 | 16:21:00 | -9.7 | -35.45 | -73.9875 | 319.5625 | 26.5 | 76.26 | | | | | | | 22.295 |
| 7/20/2016 | 16:22:00 | -3.3 | -28.9 | -51.3375 | 333.75 | 27.5 | 75.79 | | | | | | | |
| 7/20/2016 | 16:23:00 | -7.65 | -33.9 | -59.475 | 345.75 | 26.9 | 74.85 | | | | | | | 22.9125 |
| 7/20/2016 | 16:24:00 | -4 | -26.45 | -55.05 | 358.375 | 27.2 | 75.07 | | | | | | | |
| 7/20/2016 | 16:25:00 | -15.4 | -42.75 | -81.8625 | 322 | | 74.76 | | | | | | | 22.23 |
| 7/20/2016 | 16:26:00 | -8.45 | -32.95 | -66.675 | 337.9375 | | 73.4 | | | | | | | |
| 7/20/2016 | 16:27:00 16:28:00 | -17.3 | -40.7 | -81.3 | 323.6875 | | 71.4 72.42 | | | | | | | 23.02625 22.79875 |
| 7/20/2016 7/20/2016 | 16:28:00 | -8.95 -13.2 | -32.75 -39 | -64.275 -69.8625 | 339.125 316.1875 | 24.2 22.6 | 77.1 | | | | | | | |
| 7/20/2016 | 16:29:00 | -13.2 | -39 -30.65 | -69.8625 | 331.75 | | 77.62 | | | | | | | |
| 7/20/2016 | 16:31:00 | -7.55 -9.3 | | -63.6375 | | 22.4 | 76.36 | | | | | | | |
| 7/20/2016 | 16:32:00 | -3.5 | | -53.6625 | 356.875 | | 78.54 | | | | | | | |
| 7/20/2016 | 16:33:00 | -15.55 | -40.05 | -66.9375 | 322.75 | | 78.99 | | | | | | | |
| 7/20/2016 | 16:34:00 | -7,4 | -31.35 | -54.6375 | 338.8125 | 30 | 76.41 | | | | | | | |
| 7/20/2016 | 16:35:00 | -12.35 | -39.35 | -68.5875 | 327.1875 | | 75.53 | | | | | | | |
| 7/20/2016 | 16:36:00 | -5.85 | -29.6 | -61.05 | 340.6875 | | 75.34 | | | | | | | |
| 7/20/2016 | 16:37:00 | -10.6 | | -80.85 | 319.5625 | | 76.45 | | | | | | | |
| 7/20/2016 | 16:38:00 | -6.45 | -29.2 | -56.475 | 333.3125 | 25.9 | 75.92 | 7.85 | 40.06 | 11.5 | 8.68 | 1.3 | 7 892.5 | 22.9775 |
| 7/20/2016 | 16:39:00 | -6.55 | -27.4 | -58.6875 | 349.4375 | 28.8 | 76.8 | 8.02 | 40.06 | 11.3 | 8.82 | 1.15 | 5 902.2 | 22.18125 |
| 7/20/2016 | 16:40:00 | -3.7 | -26 | -47.475 | 359.0625 | . 29.2 | 77.34 | 8.1 | 40.06 | 12 | 8.63 | 1.18 | 3 912.8 | 22.76625 |
| 7/20/2016 | 16:41:00 | -12.15 | -36.55 | -63 | 328.4375 | 33.7 | 76.24 | 8.19 | 40.06 | 11.1 | . 8.54 | 1.2 | 5 928.2 | 23.01 |
| 7/20/2016 | 16:42:00 | -6.2 | -32.3 | -53.25 | 341.6875 | 30.4 | 72.61 | 8.1 | 40.06 | 11.1 | . 8.56 | 5 1.2 | 5 920.6 | 22.44125 |
| 7/20/2016 | 16:43:00 | -10.25 | -35.65 | -68.2125 | 330.375 | 27.2 | 72.16 | 8.04 | 40.06 | 10.8 | 8.66 | i 1.3: | | |
| 7/20/2016 | 16:44:00 | -5.2 | | -70.2 | | | 73.96 | | | | | | | |
| 7/20/2016 | 16:45:00 | -7.65 | | -65.5875 | 320.9375 | | 74.04 | | | | | | | |
| 7/20/2016 | 16:46:00 | -5.35 | | -64.425 | 334.5 | | | | | | | | | |
| 7/20/2016 | 16:47:00 | -8.1 | | -60.4875 | 349.125 | | | | | | | | | |
| 7/20/2016 | 16:48:00 | -1.75 | | -60.6375 | 360.6875 | | | | | | | | | |
| 7/20/2016 | | -11.3 | | | 328.375 | | | | | | | | | |
| 7/20/2016 | | | | -55.8375 | | | 71.35 | | | | | | | |
| 7/20/2016 7/20/2016 | | | | -60.075 -56.1375 | 336.875 | | | | | | | | | |
| 7/20/2016 | | | | | 347 327.0625 | | | | | | | | | |
| 7/20/2016 | | -8.05 -10.45 | | | 327.0625 | | | | | | | | | |
| 7/20/2016 | | -10.45 | | | 353.5625 | | | | | | | | | |
| 7/20/2016 | | | | -67.0125 | 355.5625 291 | | | | | | | | | |
| 7/20/2010 | | | | | | | | | | | | | | |
| 7/20/2016 | | | | | 277.8125 | | | | | | | | | |
| 7/20/2016 | | | | | | | | | | | | | | |
| 7/20/2016 | | | | | | | | | | | | | | |
| 7/20/2016 | | | | | 323.75 | | | | | | | | | |
| 7/20/2016 | | | | | 266.25 | | | | | | | | | |
| 7/20/2016 | | | | | | | | | | | | | | |
| 7/20/2016 | 17:04:00 | | | -79.425 | 263 | 23.6 | 80.26 | 8.04 | 40.06 | 11.4 | 8.73 | | | |
| 7/20/2016 | 17:05:00 | -12.2 | -37.8 | -66.075 | 330.9375 | 23.6 | 79.74 | 8.03 | 40.06 | 10.9 | 8.72 | L 1.2 | 1 906 | 22.2 |
| | Average | -11.88 | -36.98 | -64.14 | 324.50 | 25.94 | 75.14 | 8.04 | 40.06 | 5 11.24 | 8.68 | 3 1.2 | 8 904.98 | 22.5 |
| July 20, 2016 | | Pressures | | 40 40 M and an | | Analuzora | 1 | | | | | | | Flows |
| July 20, 2010 | | Incinerator | | SD Outlet | Baghouse | Analyzers CO | НСІ | CO2 | H20 | ТНС | 02 | Opacity | SO2 | PACFlow |
| Test1 | 20-345 #2070204 Auronautor | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC-FT |
| | | | | | | | | | | | | | | |

| July 20, 2016 | Pressures | · · · | | | Analyzers | | | | | | | | Flows |
|---------------|-------------|-----------|-----------|----------|-----------|----------|----------|----------|----------|----------|----------|----------|-----------|
| | Incinerator | SDA Inlet | SD Outlet | Baghouse | со | HCI | CO2 | H2O | THC | 02 | Opacity | SO2 | PACFlow |
| Test1 | PT-242A | PT-249 | PT-615 | PDT-622 | AT-205 | AT-213A | AT-213B | AT-213C | AT-259 | AT-261 | AT-263 | AT-264 | SC-PAC-FT |
| Max | -1.8 | -24.2 | -45.0 | 360.7 | 33.7 | 80.3 | 8.2 | 40.1 | 12.0 | 8.9 | 1.4 | 933.1 | 23.0 |
| Min | -31.7 | -60.5 | -81.9 | 256.7 | 21.7 | 69.9 | 7.9 | 40.1 | 10.4 | 8.4 | 1.1 | 883.5 | 22.2 |
| Average | -11.9 | -37.0 | -64.1 | 324.5 | 25.9 | 75.1 | 8.0 | 40.1 | 11.2 | 8.7 | 1.3 | 905.0 | 22.6 |
| Variance | 69.45525 | 104.7543 | 85.02251 | 783.9182 | 6.350486 | 6.856213 | 0.008823 | 1.85E-27 | 0.174011 | 0.014703 | 0.007931 | 146.3547 | 0.0882699 |